

# Granular Mechanics of Geomaterials

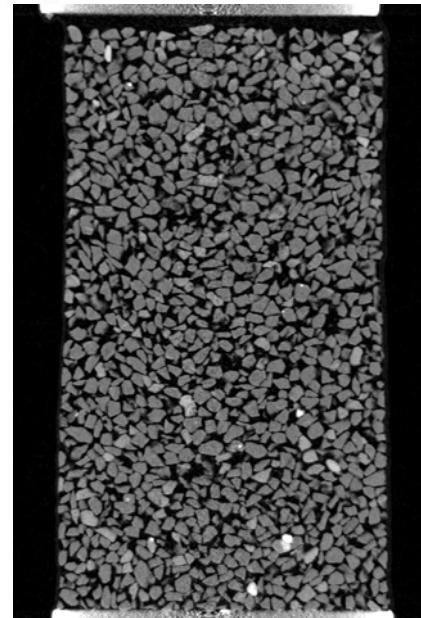
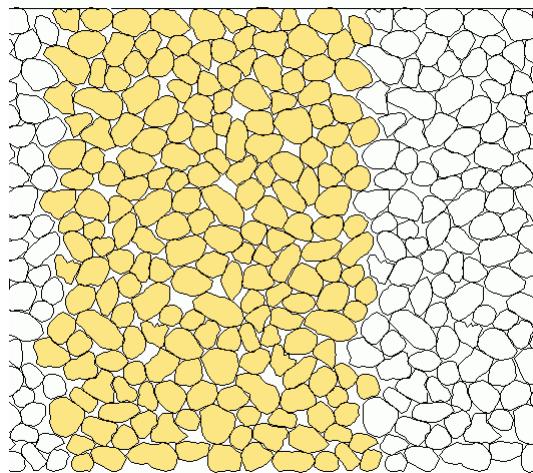
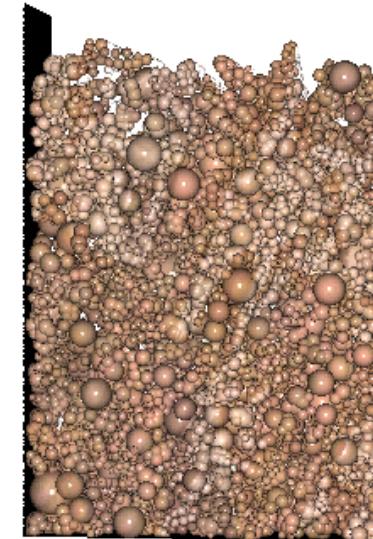
(presentation in Cassino, Italy, 2006)

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Takashi Matsushima

University of Tsukuba

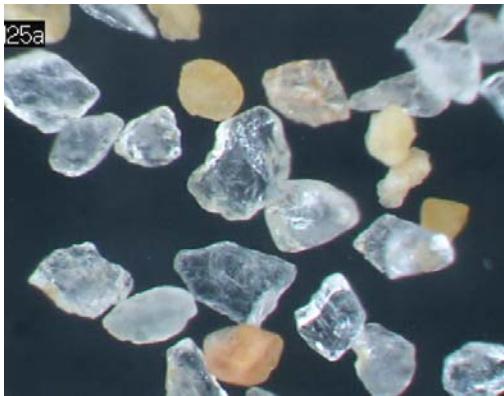


# Where am I from?

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# What is granular mechanics?



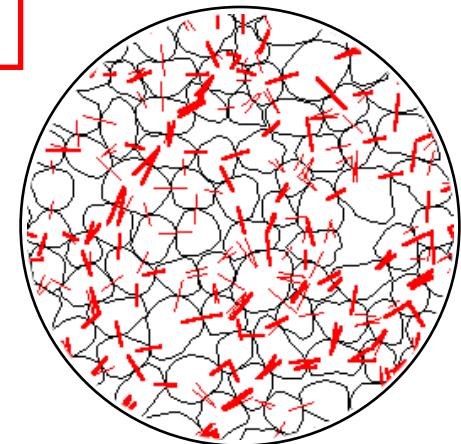
**Particle characteristics**  
(size, shape, crushability etc.)

**Particle interaction**

**Direct simulation**  
(by DEM etc.)

**Constitutive model as  
solid or fluid**

**No element test!?**



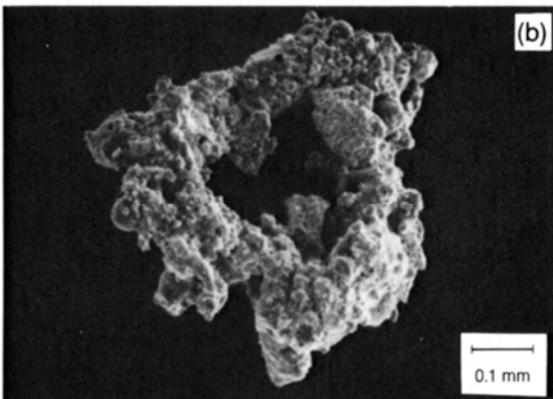
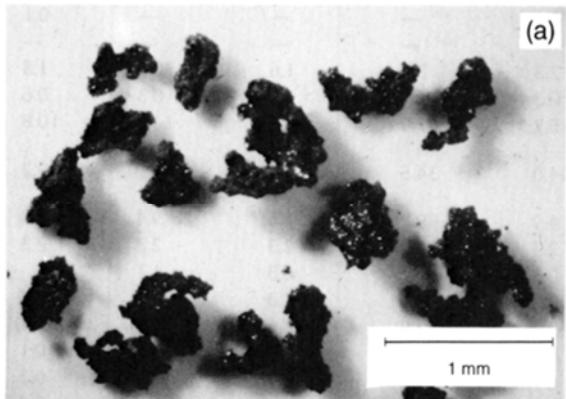
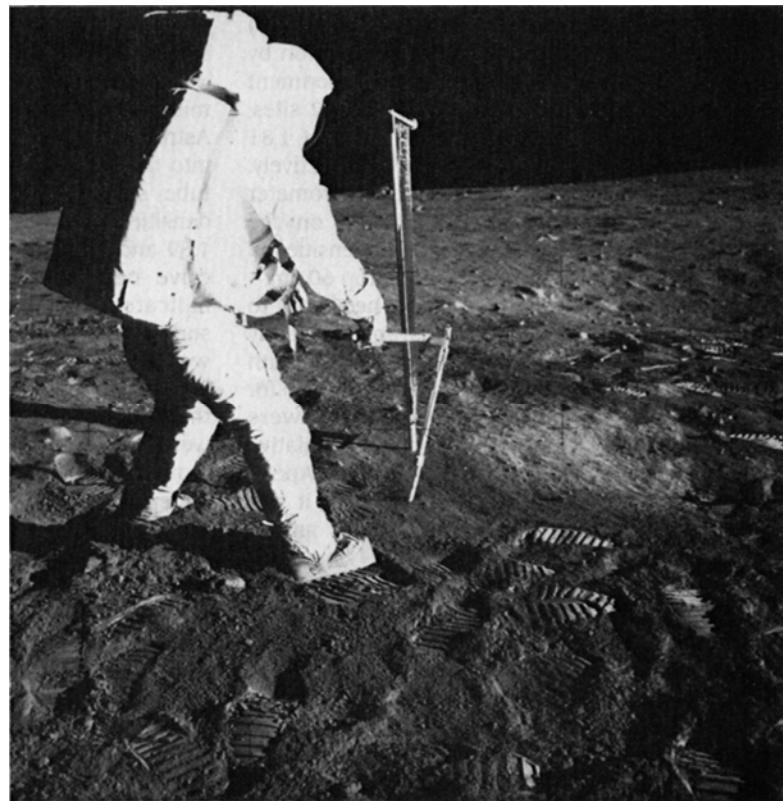
**Simulation as continua  
(by FEM, SPH etc.)**

# Lunar exploration

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Mechanical properties  
of Lunar soil is needed.

But only TWO **TC** test  
results is available.



Lunar regolith:  
very angular  
well graded sand

Lunar sourcebook, 1991

# Why granular mechanics?

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\***TRUE** prediction  
from particle information

eg.

Mechanics of crushable soil

Mechanics of unsaturated soil

Mechanics of cemented soil

and more...

\***UNIQUE** constitutive model  
more convincing, more rational

# **Contents:**

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## **1. Theory of granular mechanics**

**Chang and Misra 1990, Matsushima and Chang 2006**

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## **2. Micro X-ray CT experiment**

**Matsushima et al. 2002-**

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## **3. Image-based DEM simulation**

**Matsushima 2002-**

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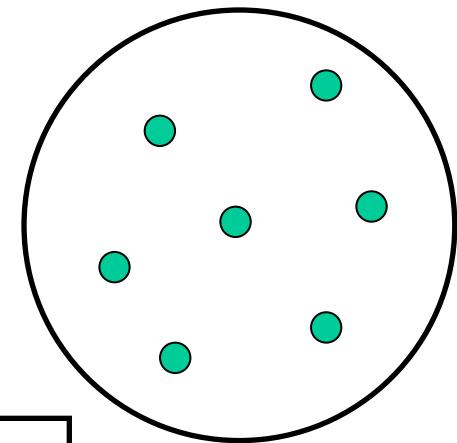
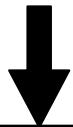
incl. recent application to Lunar exploration

**Matsushima 2006**

# Basic theories

Molecular dynamics

**Statistical mechanics** for molecules  
(sparse, non-frictional )

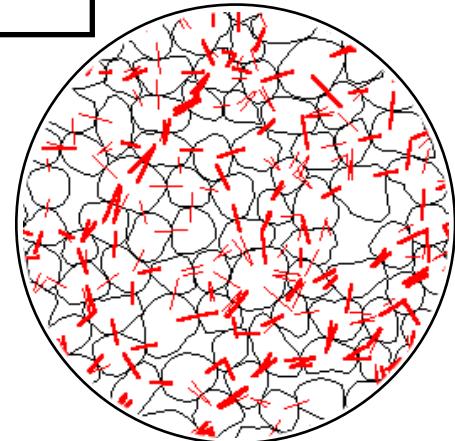


Mechanics of solid **frictional** particles

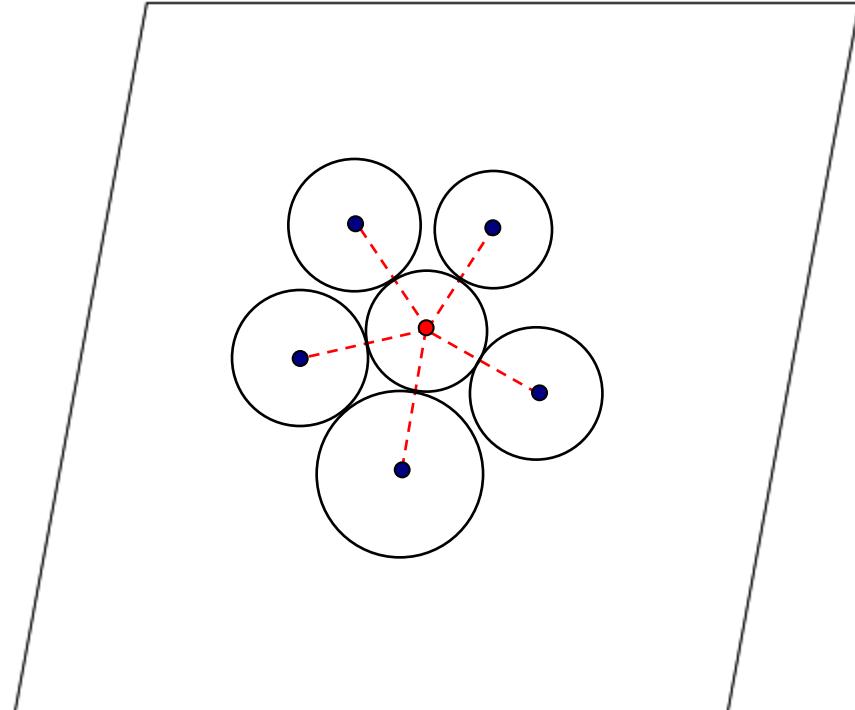
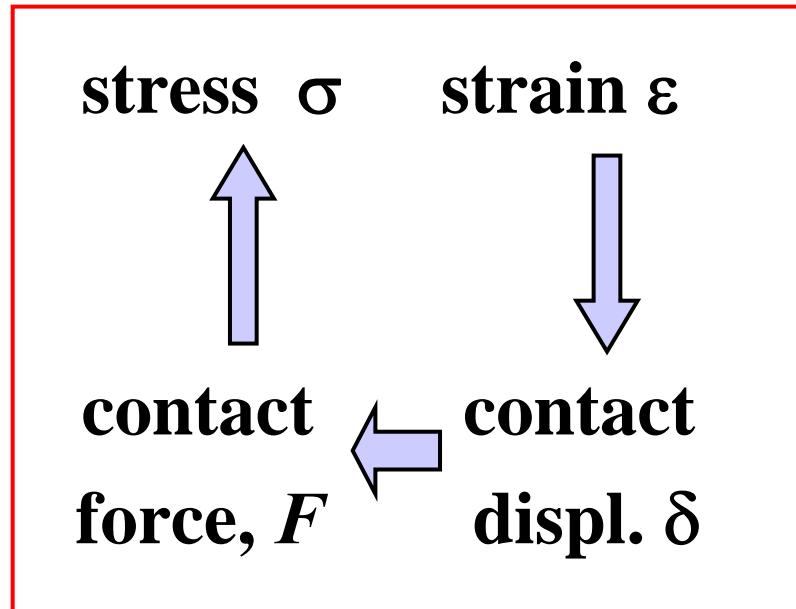
Kinetic theory  
(sparse → behaves as a **fluid**)

+

Mechanics of **geomaterials**  
(dense → behaves as a **solid**)



# Uniform strain model (Chang and Misra 1990)



- \*Grain centroids stick to continuum deformation field
- \*Grain rotation coincides with continuum rotation  
→ contact displ.  $\delta$

# Contact displ. → Contact force → Stress

Global → local coordinates

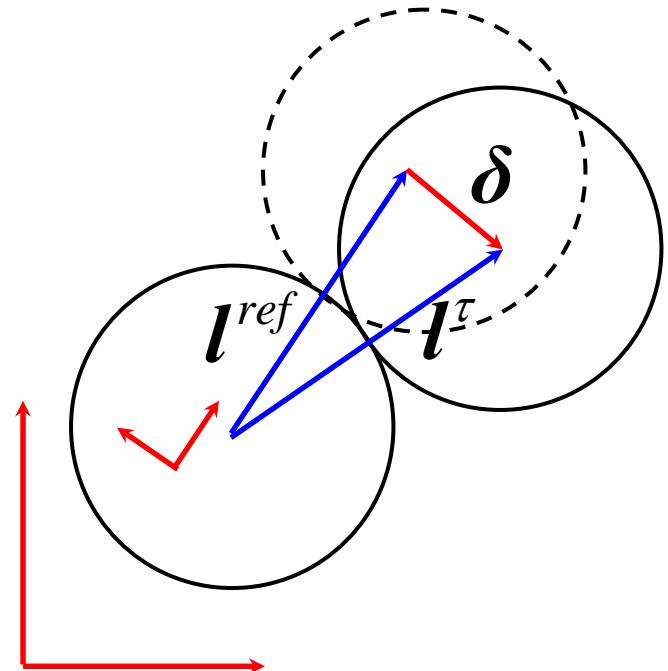
$$\boldsymbol{\delta}^L = \mathbf{R}^T \cdot \boldsymbol{\delta}$$

Force-displ. relation at contact

$$\mathbf{f}^L = \begin{pmatrix} f_n \\ f_s \end{pmatrix} = \begin{pmatrix} k_n & 0 \\ 0 & k_s \end{pmatrix} \cdot \boldsymbol{\delta}^L$$

Global local coordinates

$$\mathbf{f} = \mathbf{R} \cdot \mathbf{f}^L$$



Stress

Sum of contacts in VR

$$\boldsymbol{\sigma}^{tT} = \frac{1}{V_R^t} \sum_c (\mathbf{l}^t \otimes \mathbf{f}^t)$$

work at contact = work as continuum

# Elastic solution

Assuming  
equal-sized isotropic sphere packing...

$$\bar{E} = \frac{2r^2 N}{15V} (2k_n + 3k_s) \left( \frac{5k_n}{4k_n + k_s} \right)$$

$$\bar{\nu} = \frac{k_n - k_s}{4k_n + k_s}$$

*e-n* relation is necessary

$$\frac{N}{V} = \frac{3n}{4\pi r^3 (1+e)}$$

*n* : coordination number

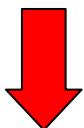
Overall Young's modulus and Poisson ratio  
can be described by contact stiffness

# Elastic solution (continued..)

Applying Hertz-Mindlin contact law... (Johnson, Contact mechanics)

$$\dot{f}_n = \left( \frac{\sqrt{3r} G}{1-\nu} \right)^{2/3} f_n^{1/3} \dot{\delta}_n \equiv k_n \dot{\delta}_n$$

$$\dot{f}_s = \frac{2(1-\nu)}{2-\nu} k_n \left( 1 - \frac{f_s}{f_n \tan \phi_\mu} \right)^{1/3} \dot{\delta}_s \equiv k_s \dot{\delta}_s$$



$$\bar{E} = \frac{2r^2(5-4\nu)}{3(5-3\nu)} (9\sigma_0)^{1/3} \left[ \frac{GN}{(1-\nu)V} \right]^{2/3}$$

$$\bar{\nu} = \frac{\nu}{2(5-3\nu)}$$

$$\bar{G} = \frac{\bar{E}}{2(1+\bar{\nu})} = A \cdot \left( \frac{n(e)}{1+e} \right)^{2/3} (\sigma_0)^{1/3}$$

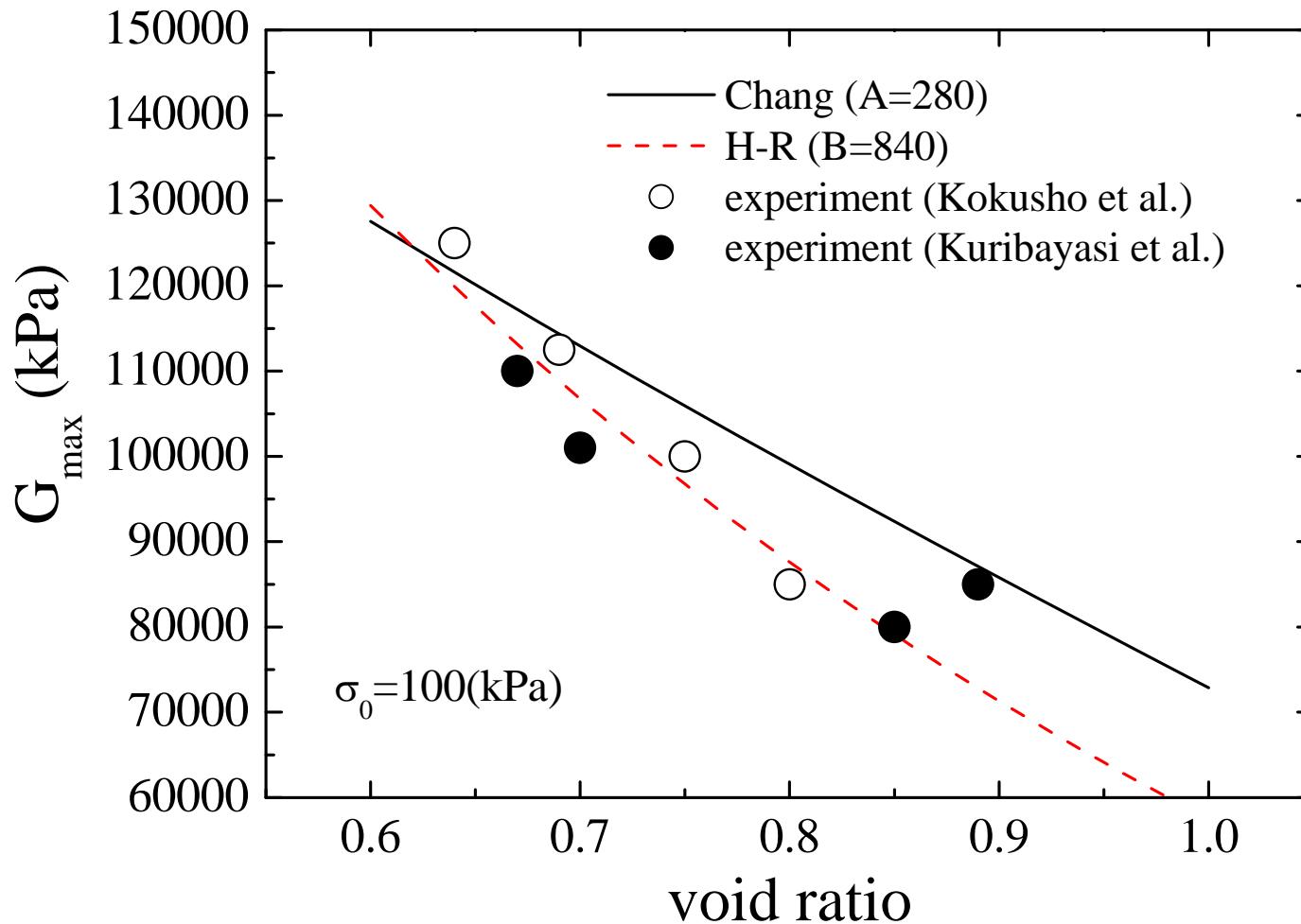
$$n(e) = 2.63 - 1.79e$$

$\bar{G}$  is a function of  
confining pressure,  $\sigma_0$   
and void ratio,  $e$

$$A = \frac{2r^2(5-4\nu)}{15(2-\nu)} (9)^{1/3} \left[ \frac{3G}{4\pi r^3(1-\nu)} \right]^{2/3}$$

Smith et al. (1929) by the combination of closest and loosest packing 11

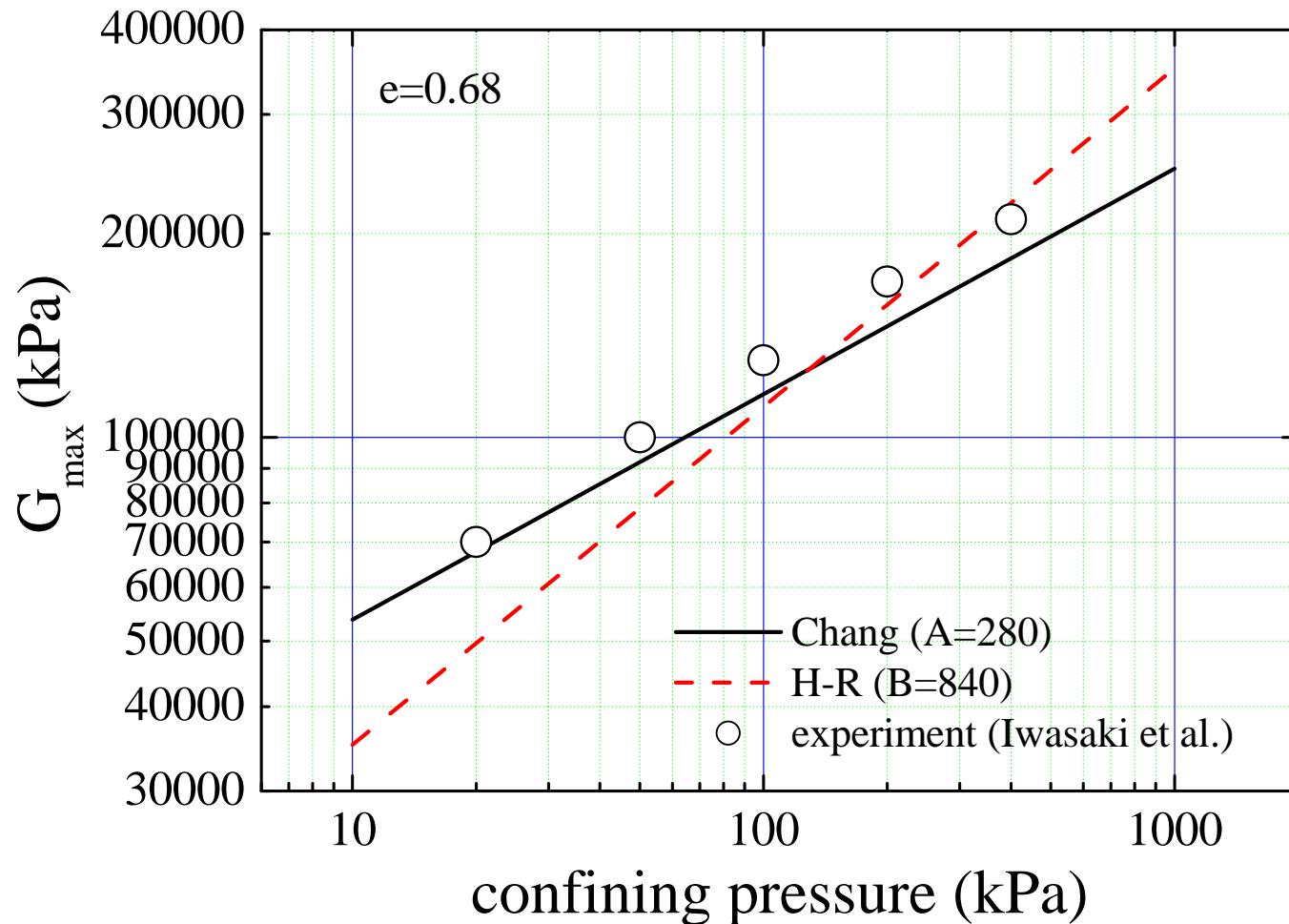
# Elastic solution (continued..)



Cf. Hardin & Richart

$$\bar{G} = B \cdot \frac{(2.17 - e)^2}{1 + e} (\sigma_0)^{1/2}$$

# Elastic solution (continued..)



Cf. Hardin & Richart  $\overline{G} = B \cdot \frac{(2.17 - e)^2}{1 + e} (\sigma_0)^{1/2}$

*Note:*

$A=280$  corresponds to

$G=73(\text{GPa})$ ,  $\nu=0.25$  (sand particle as a solid)

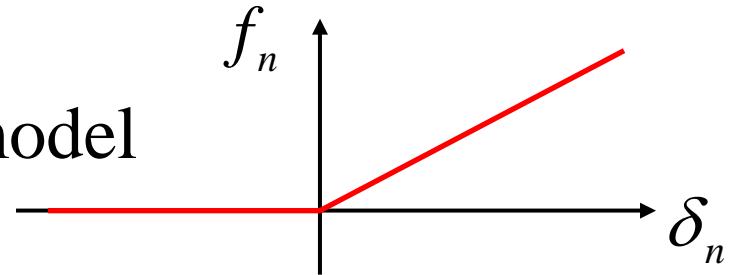
Estimation of  $\bar{\nu}$  is not good.

(Further research is necessary.)

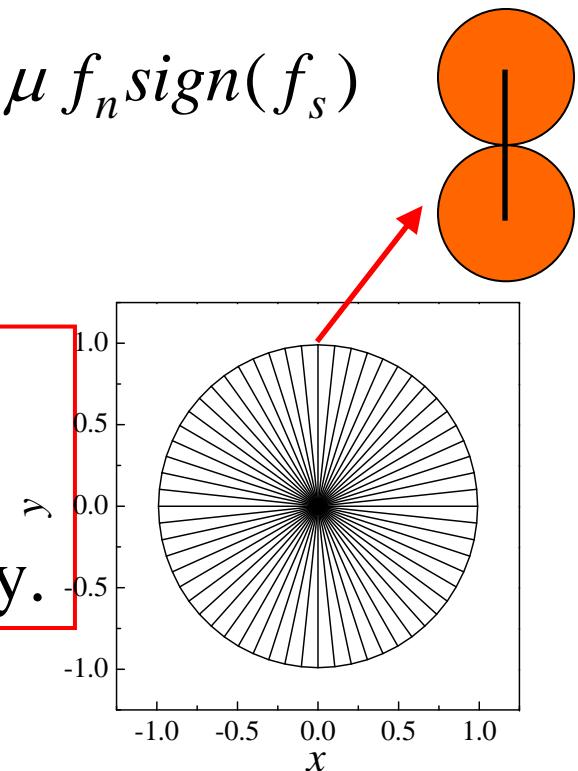
# Nonlinear model

- Loss of contact  
is considered by tension-free model
- Contact slip (plasticity)

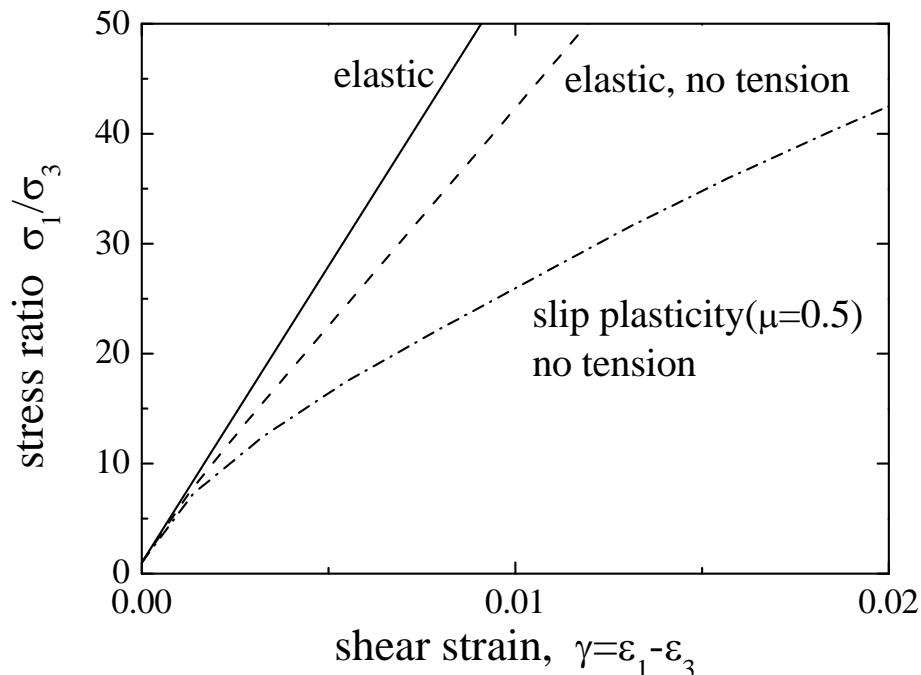
$$|f_s| \begin{cases} \leq -\mu f_n & \rightarrow (\text{elastic}) \\ > -\mu f_n & \rightarrow (\text{sliding}) \rightarrow |f_s| = -\mu f_n \text{sign}(f_s) \end{cases}$$



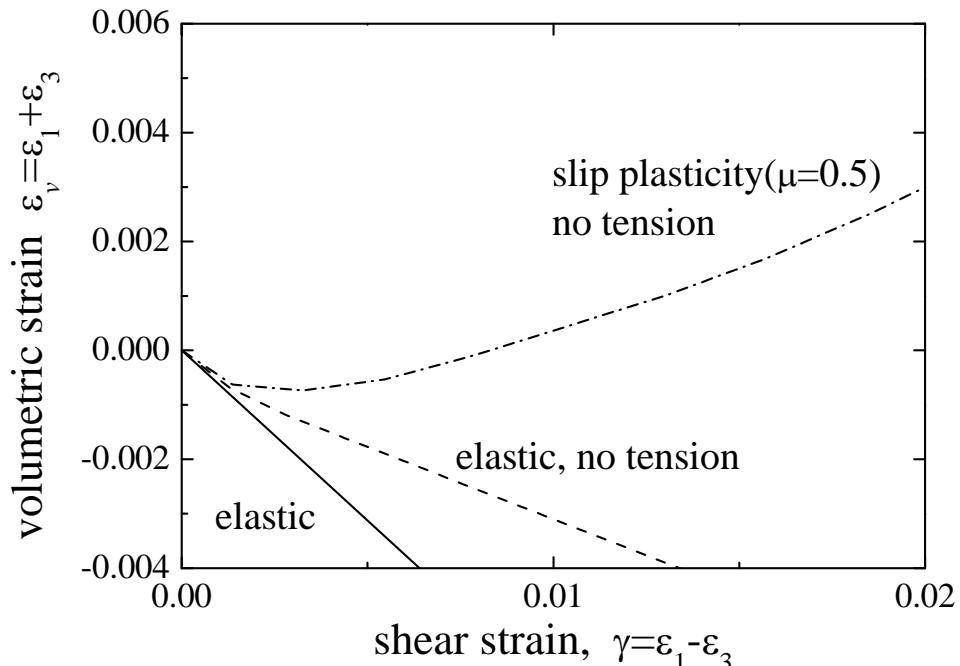
Analytical solution is not available.  
→ A set of branch vectors are assumed  
and the solution is obtained numerically.



# Basic response (biaxial compression)



stress-strain curve



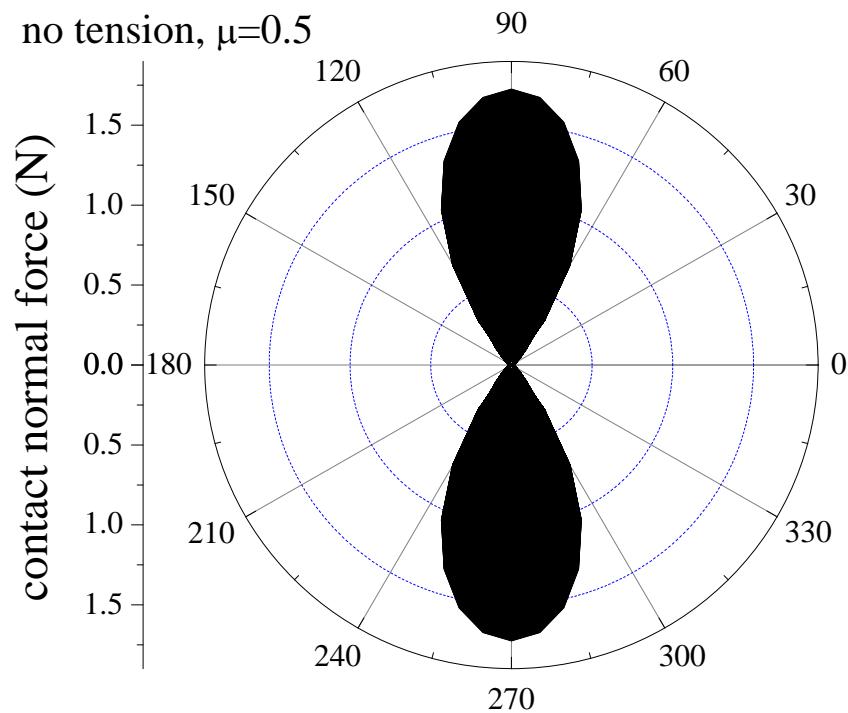
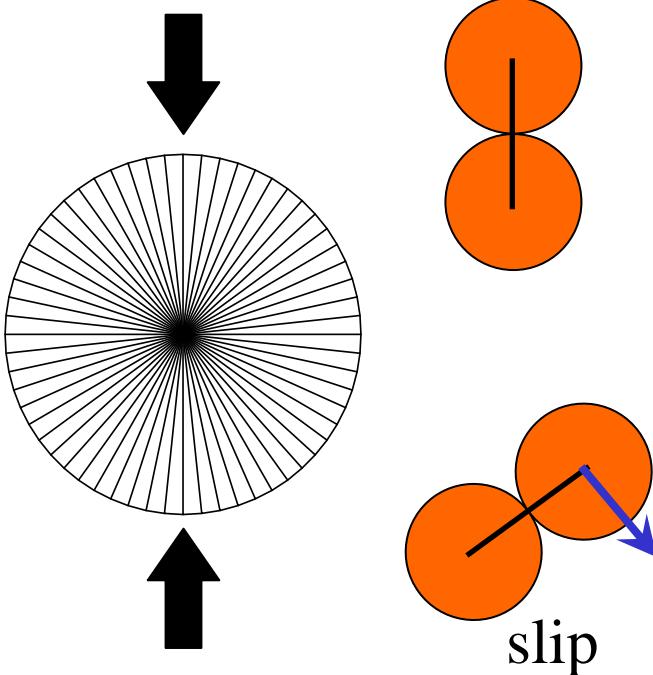
dilation curve

Material does NOT yield!

# Basic response (biaxial compression)

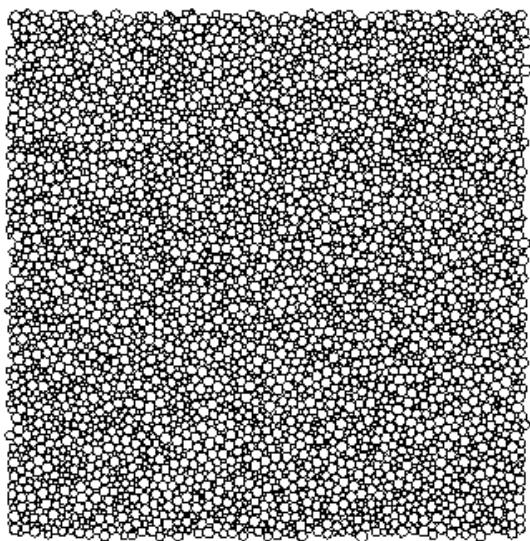
Why?

Contact of loading direction does NOT slip.

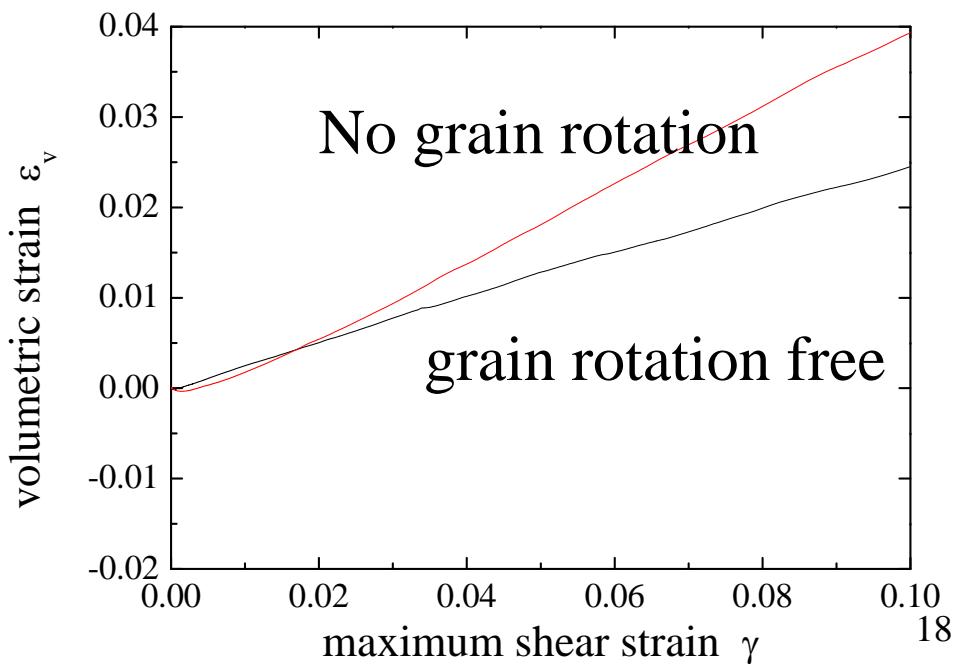
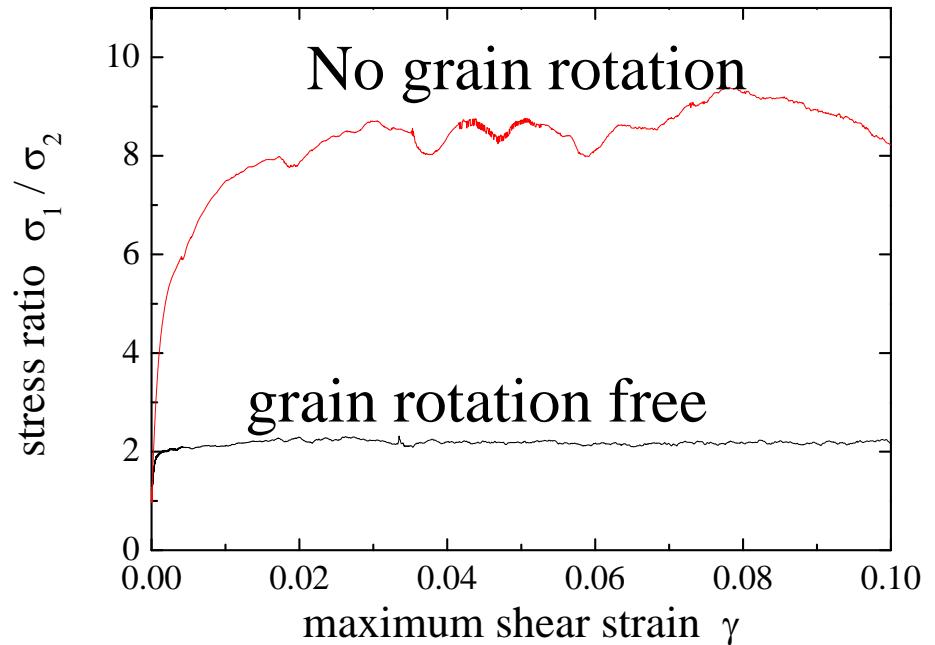


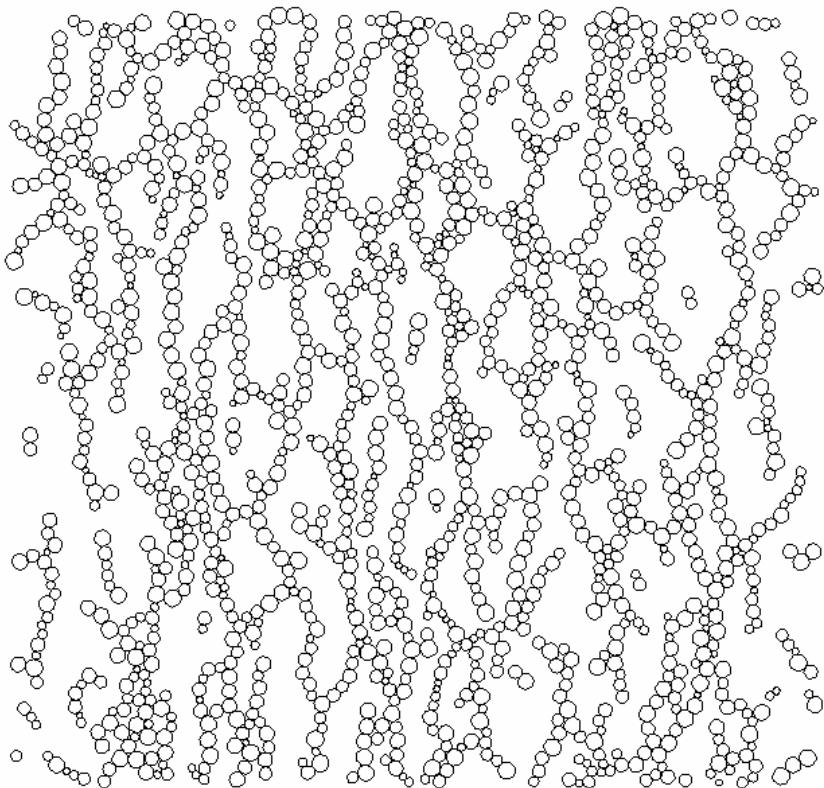
Contact normal force distribution

# DEM study

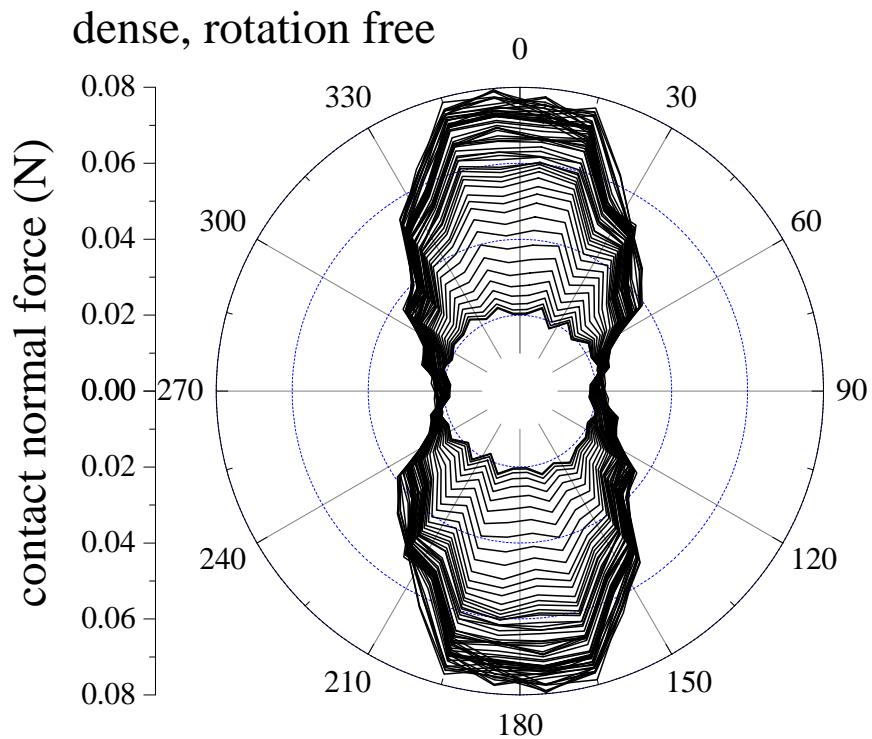


periodic boundaries  
at both directions



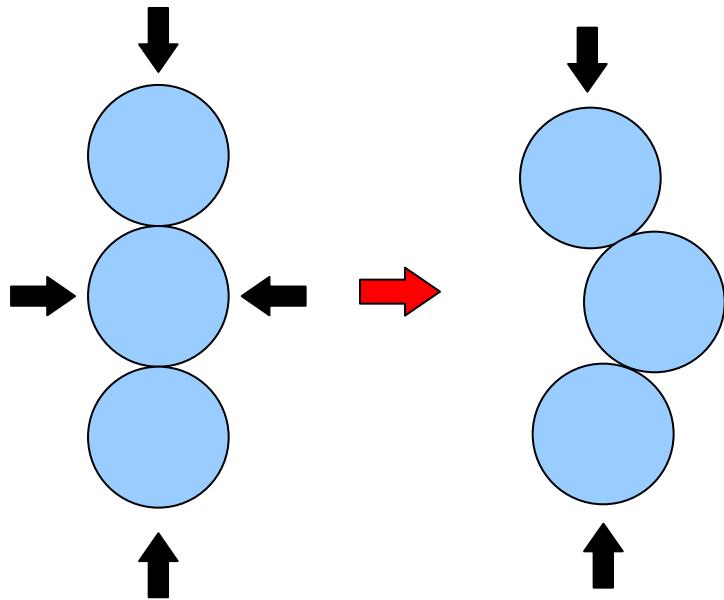


Force chain  
in granular assembly



Contact normal force  
distribution

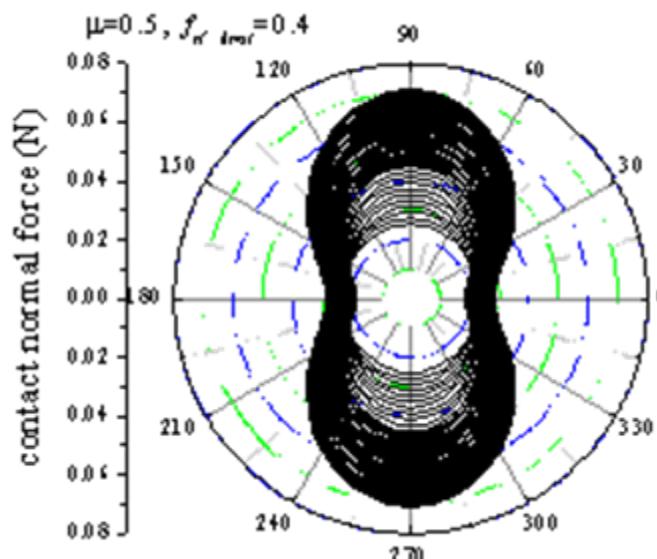
# Buckling of granular column



(Matsushima and Chang, 2006)

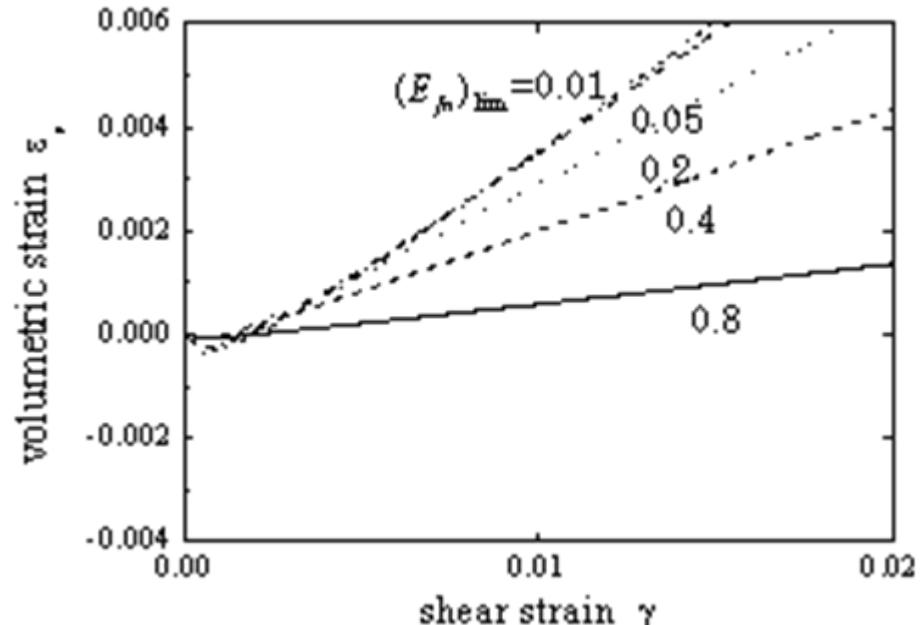
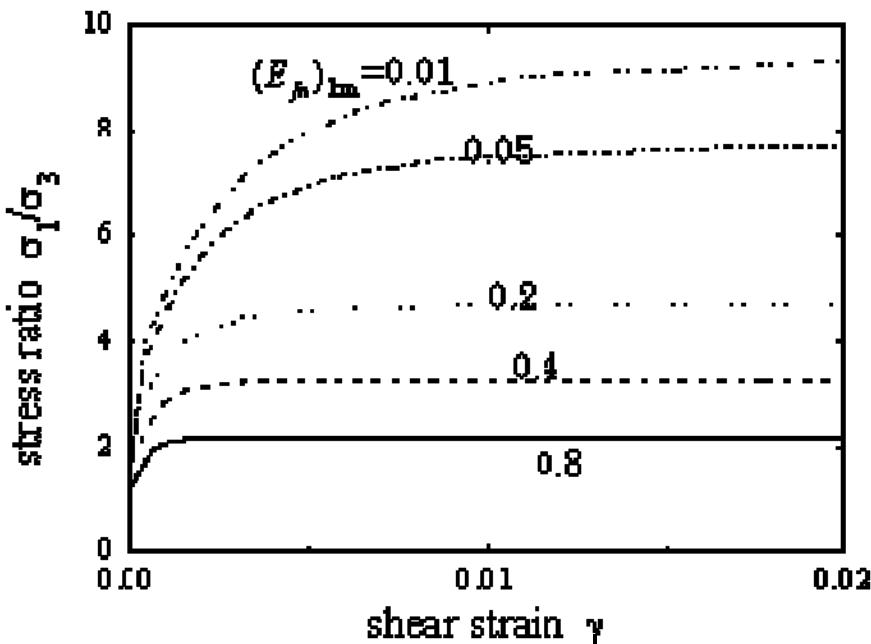
- Assign minimum aspect ratio for contact force distribution
- Determine average contact force such that the stored energy in contact keeps constant

insufficient confining  
pressure  
↓  
buckling



# Response of Buckling model

(Matsushima and Chang, 2006)



**Buckling resistance controls the yield strength**

related to particle properties

# Possibility of granular mechanics C.E.

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Rational incorporation of particle properties  
(size, shape, stiffness, crushability, contact cement, etc.)

Validation not only with macro response  
but also with particle-level information

Detailed comparison with  
**Particle visualization experiment**  
**More realistic DEM**  
is needed.

# Particle visualization by Micro X-ray CT

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At University Joseph Fourier, Grenoble, 2002

**to obtain 3-D micro properties  
(grain properties, microstructure  
and its change due to external loading)  
of some standard sands  
with micro X-ray CT in SPring-8**

**Typical standard sands:**

**Toyoura sand:  $D_{50} = 0.167\text{ (mm)}$**

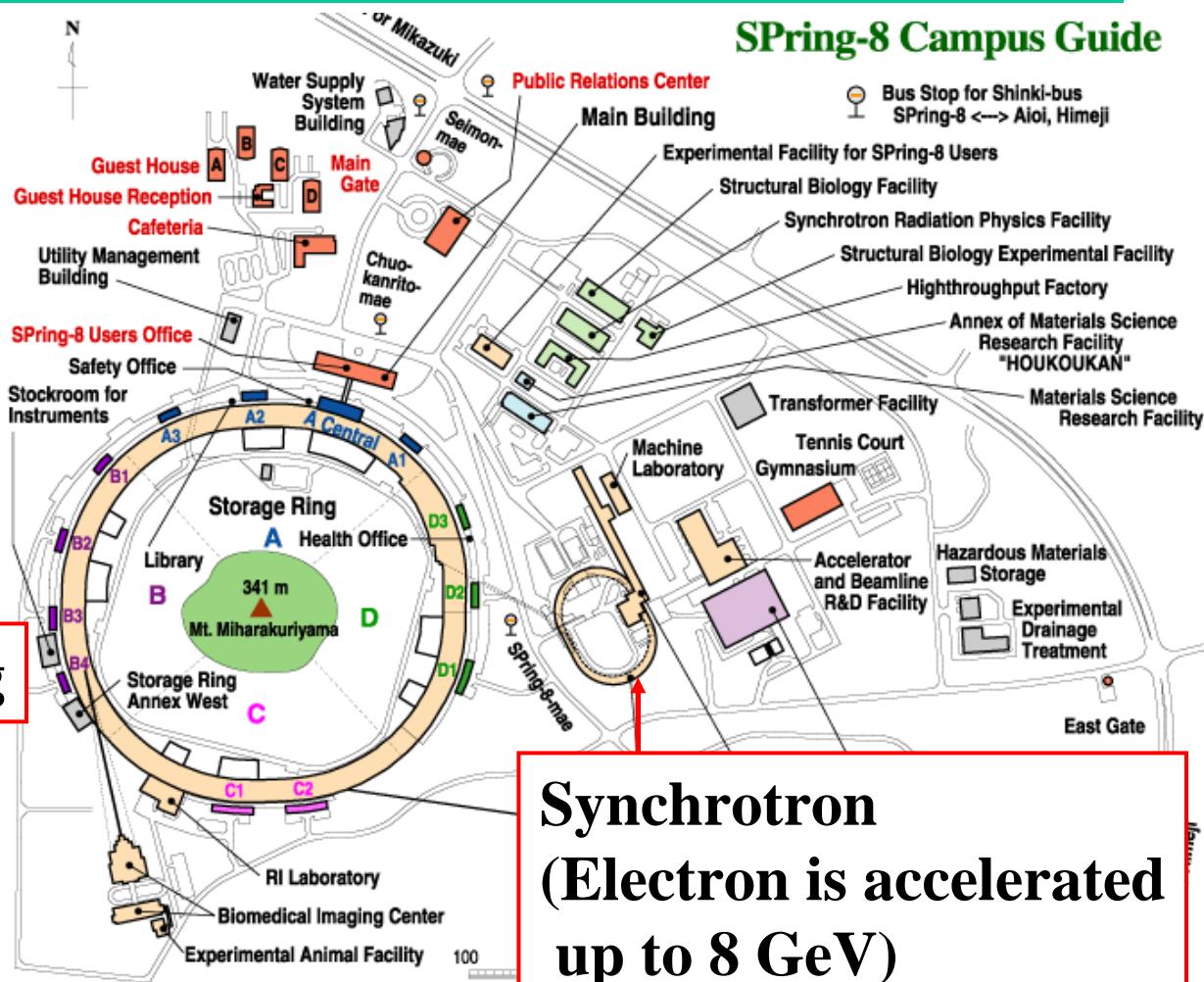
**Ottawa sand:  $D_{50} = 0.174\text{ (mm)}$**

**Hostun sand:  $D_{50} = 0.408\text{ (mm)}$**

**S.L.B. sand:  $D_{50} = 0.681\text{ (mm)}$**

**(high resolution system is necessary)**

# Micro X-ray CT at Spring-8

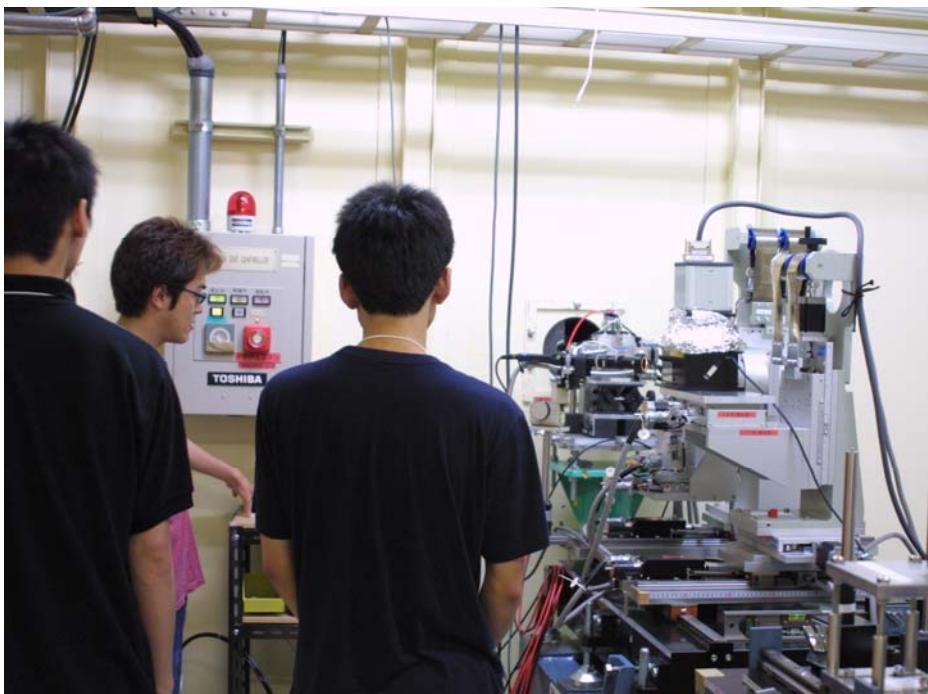


The world's largest third-generation synchrotron radiation facility

# Storage ring facility



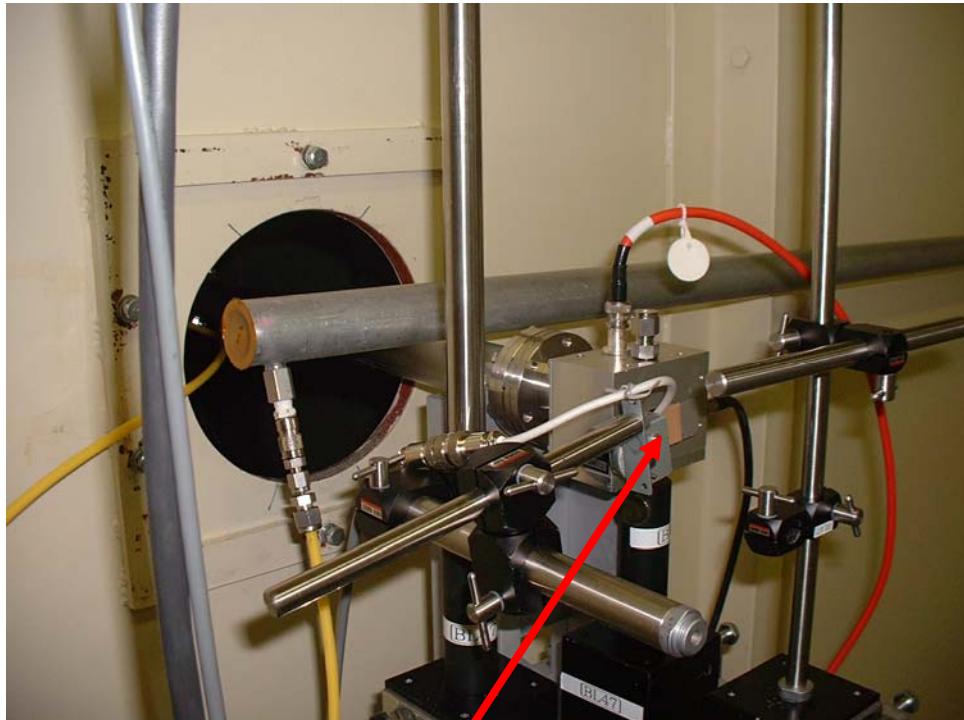
# Experimental room



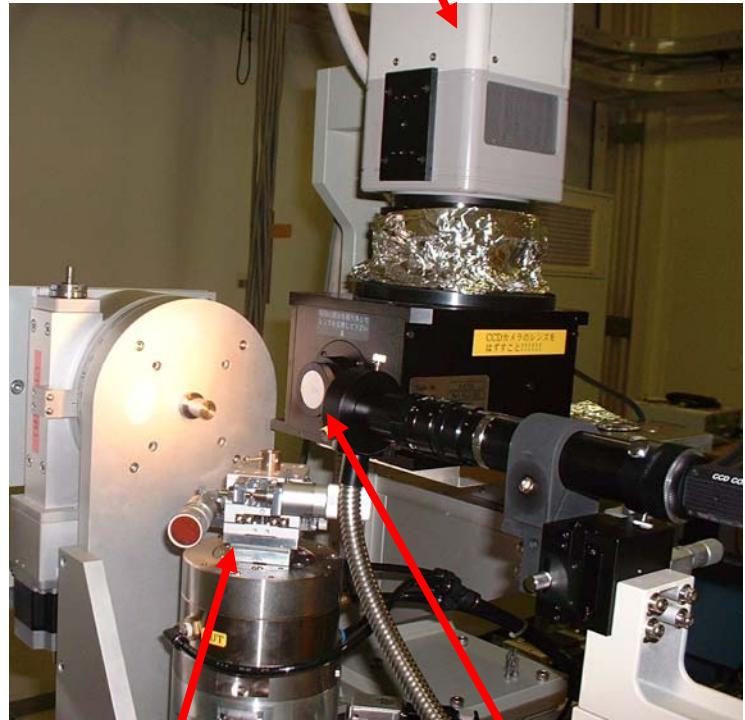
**47 beamlines (BL)**

**X-ray CT is available at  
BL20B2 and BL47XU.**

# Outline of Spring-8

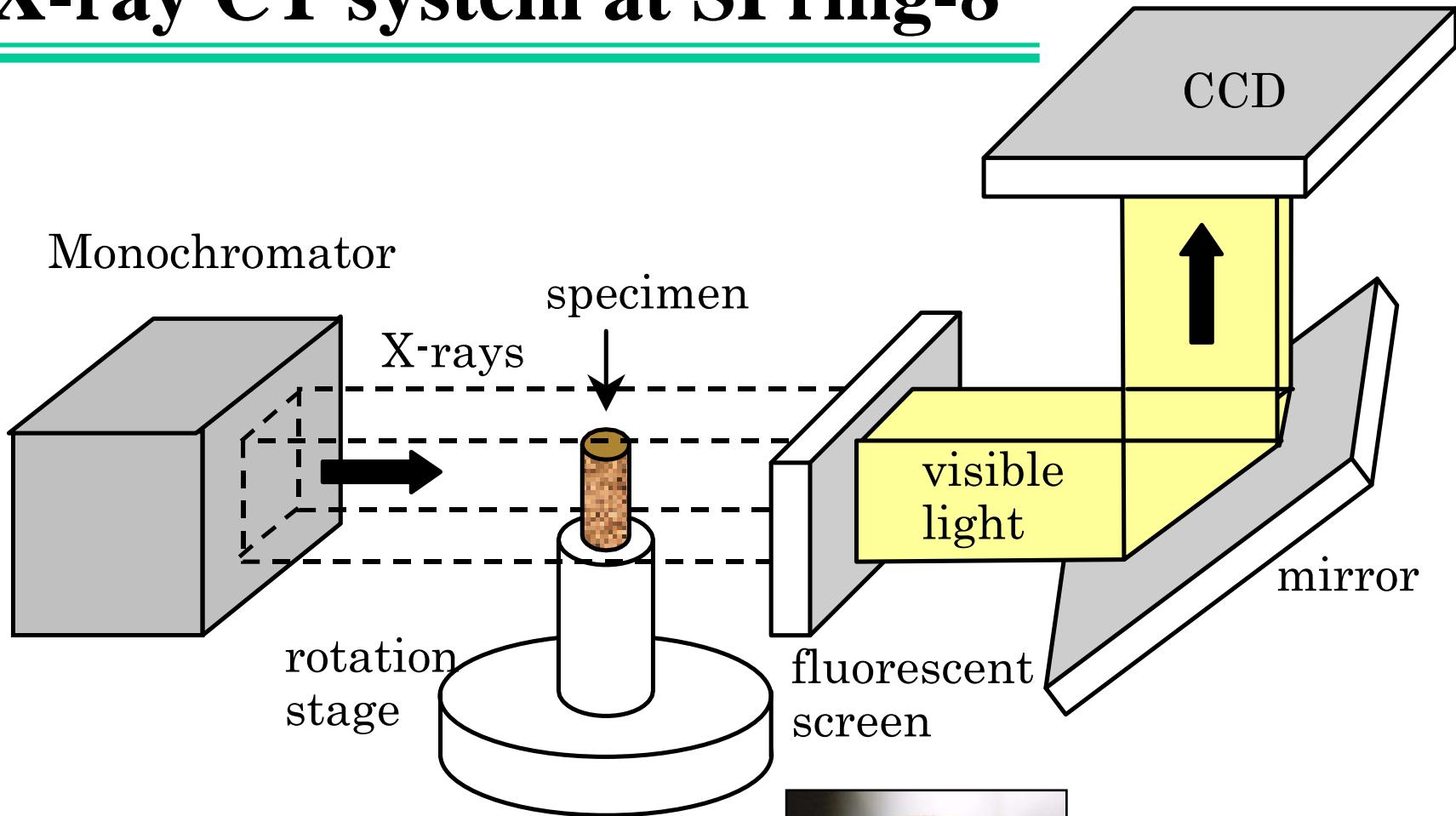


X-ray comes from here



CCD camera  
Stage  
Detector

# X-ray CT system at SPring-8

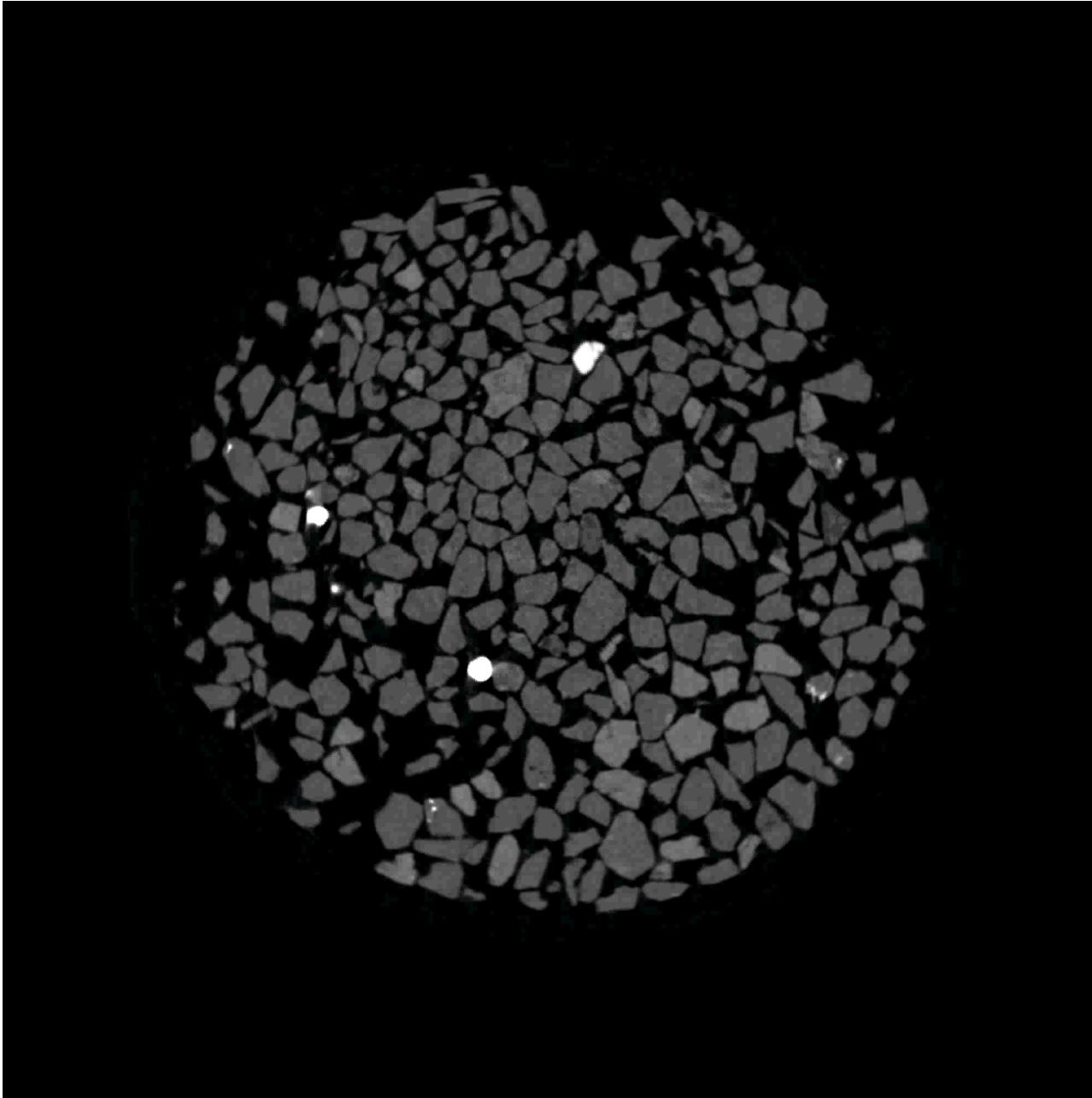


**Resolution:**

**BL20B2: 13  $\mu\text{m}$**

**BL47XU: 1.5  $\mu\text{m}$**



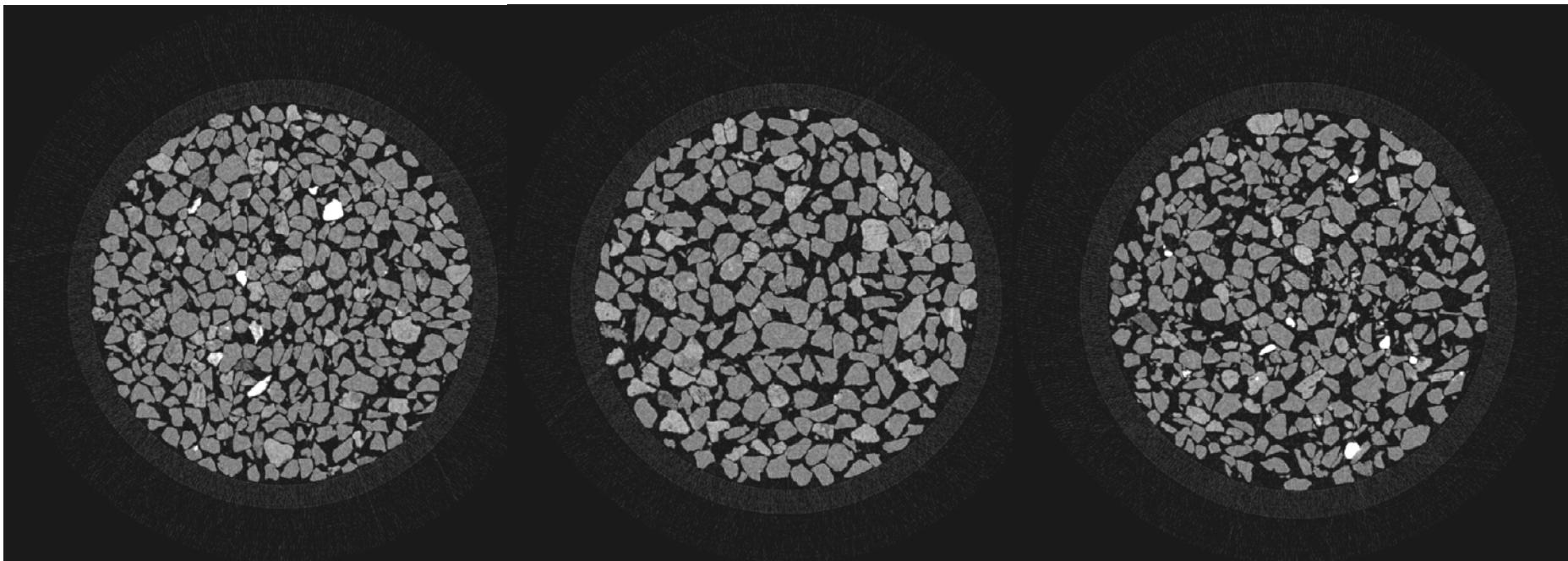


Toyoura sand      dense

# Example of CT image (BL20B2)

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Toyoura sand



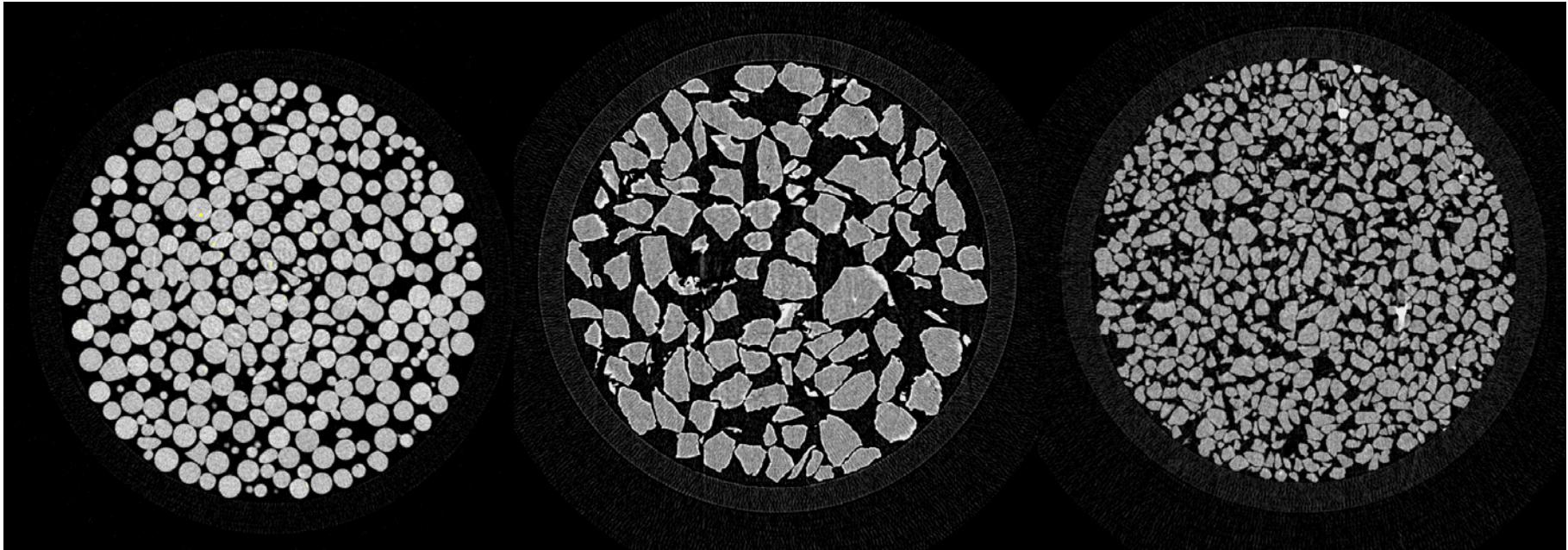
dense

medium dense

loose

# Example of CT image (BL20B2)

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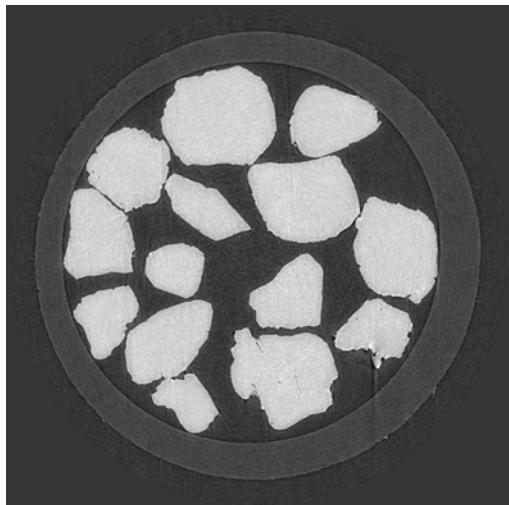


Glass beads

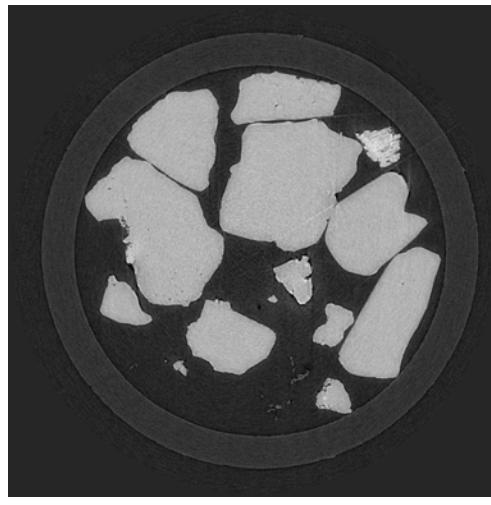
Hostun sand

Ottawa sand

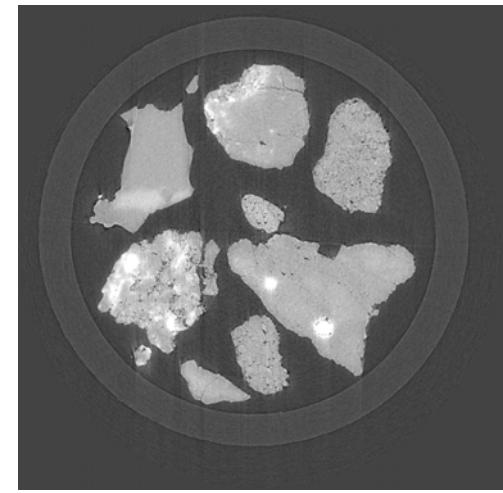
# Example of CT image (BL47XU)



Ottawa sand



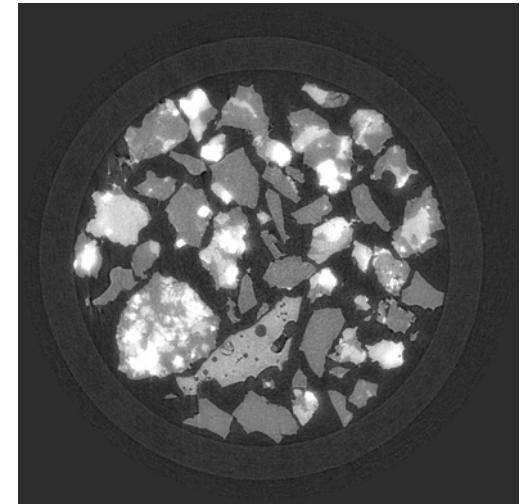
Toyoura sand



Wakasa sand

Roundish

very angular

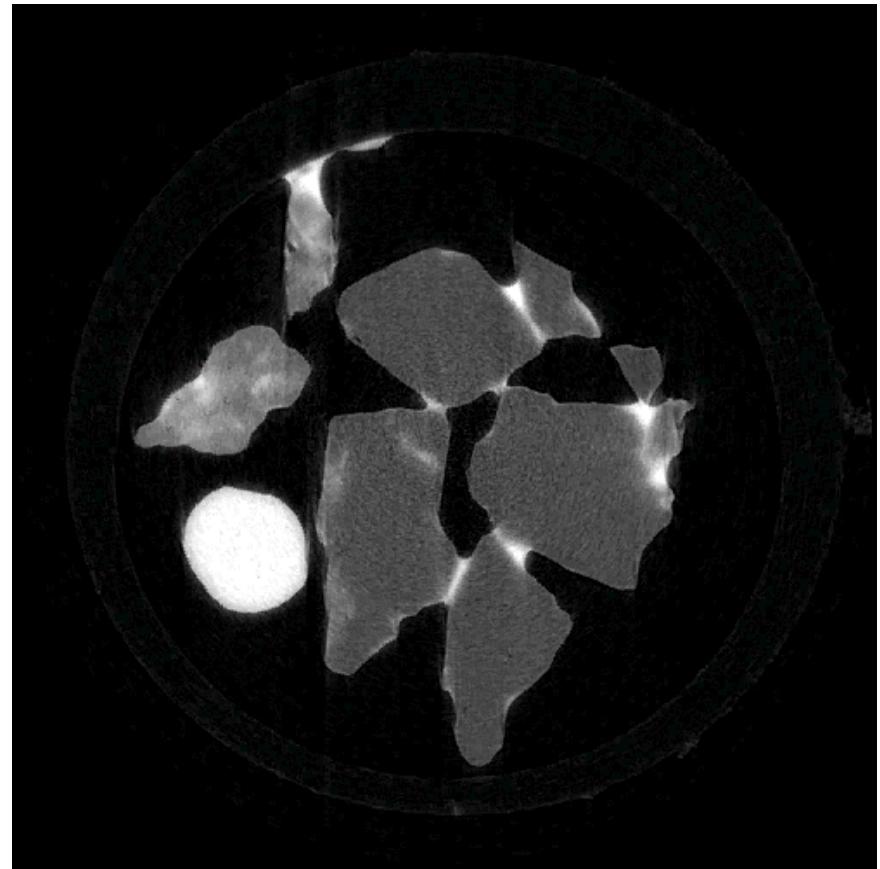


Lunar soil simulant(FJS-1)<sub>32</sub>

# Example of CT image (BL47XU)

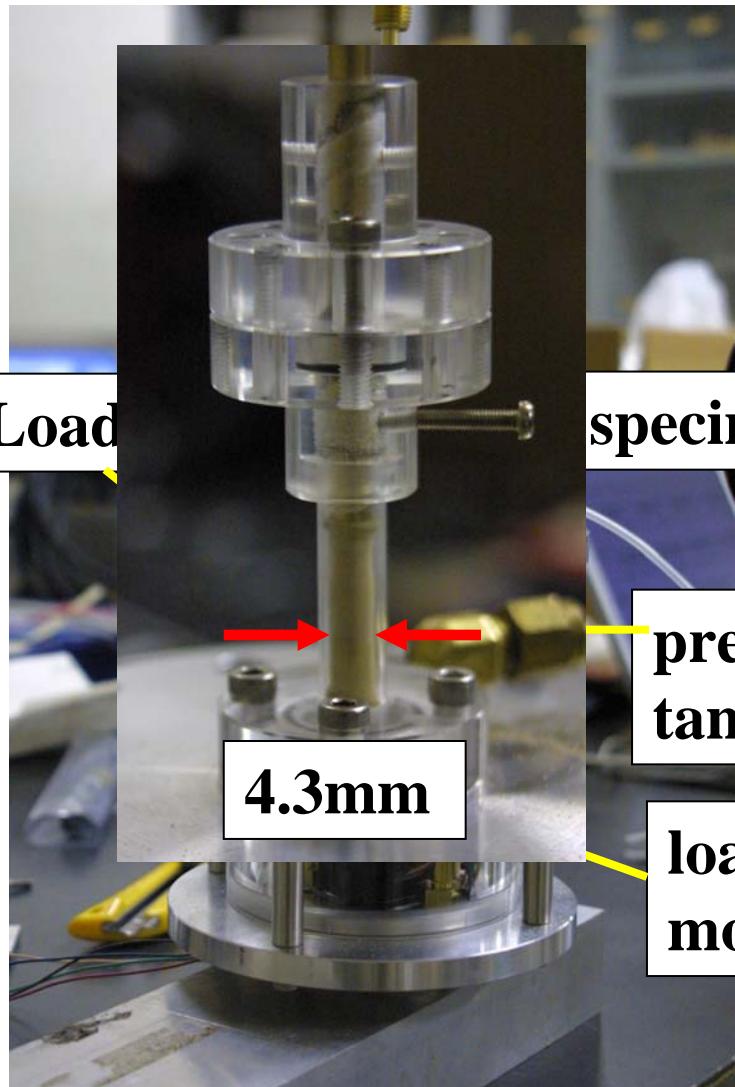


**Masado (crushable sand)**



**unsaturated condition**

# Micro Triaxial test (BL20B2)(1)



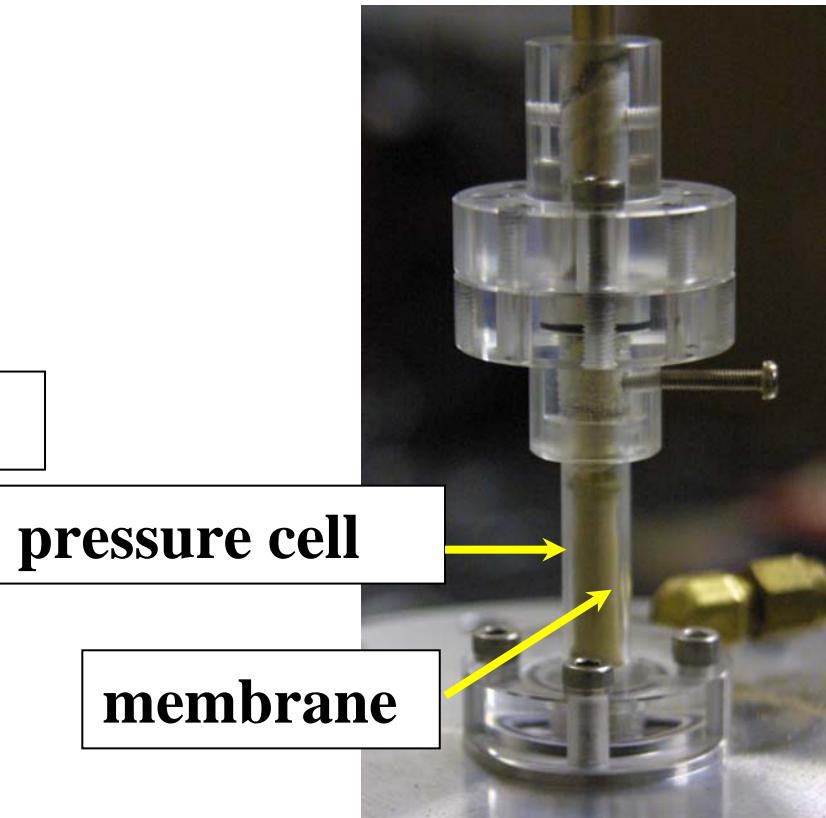
Load

specimen

4.3mm

pressure  
tank

loading  
motor



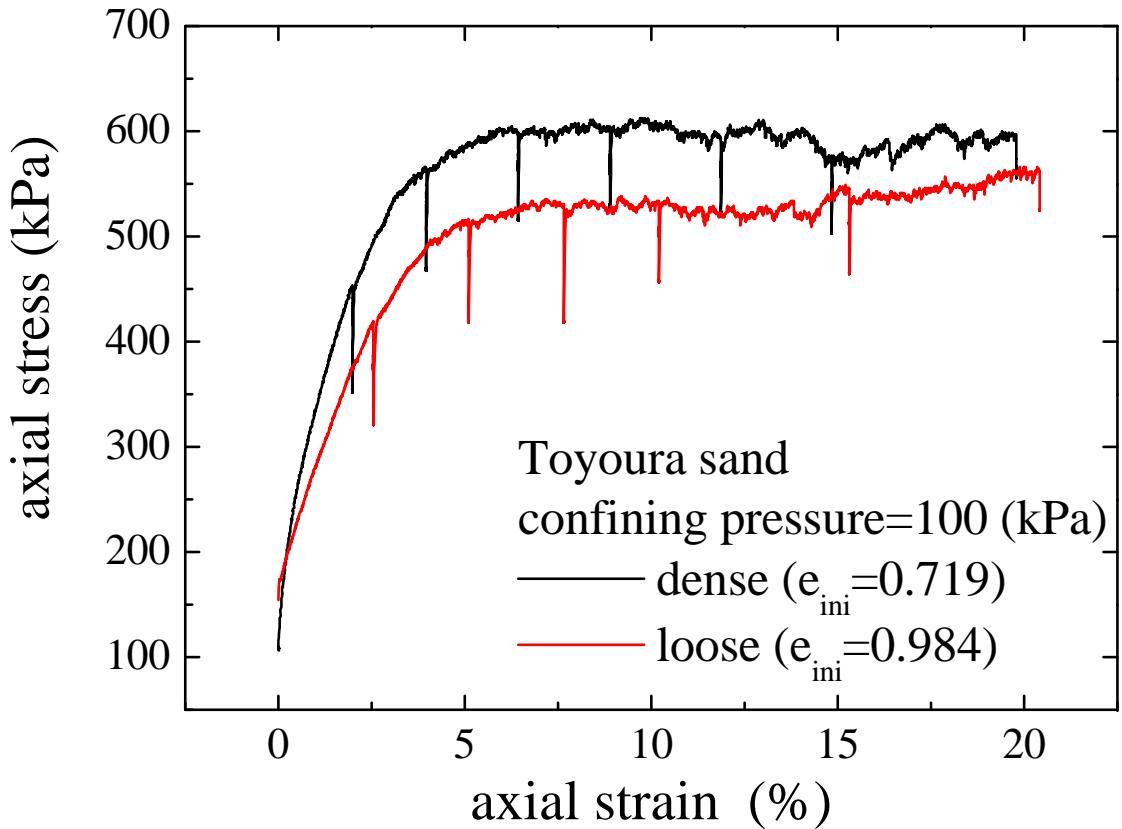
pressure cell

membrane

specimen  
diameter      4.3mm  
height            10mm

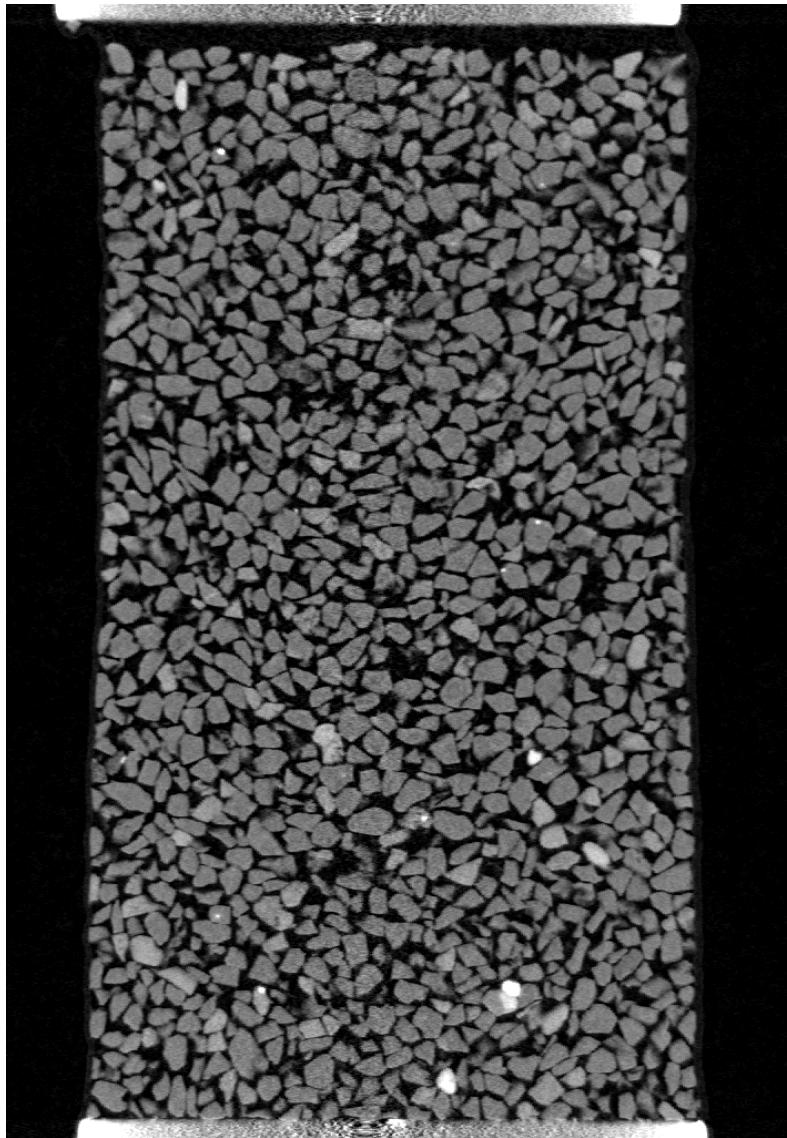
# Micro Triaxial test (BL20B2)(2)

CT scan of initial condition  
↓  
loading ←  
↓  
stop loading and CT scan (1.5 hours)



stress-strain curve

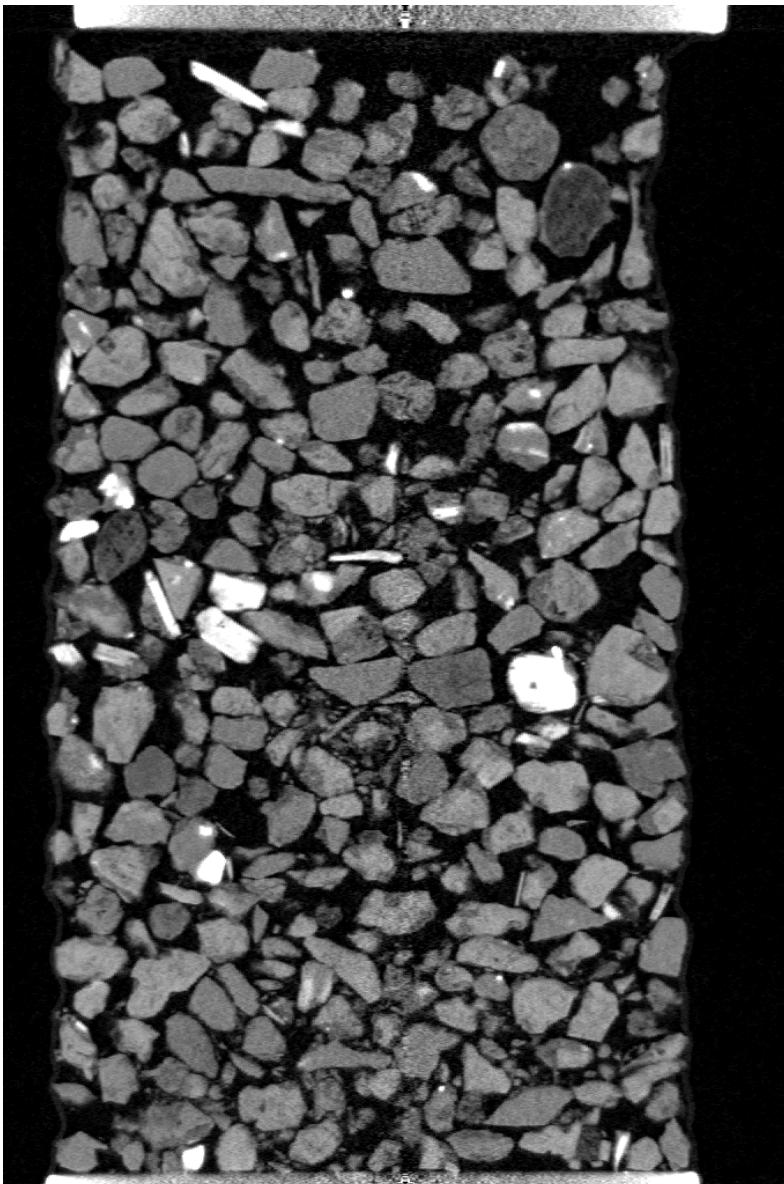
# Micro Triaxial test (BL20B2)(3)



Toyoura  
(medium dense)

void increase within  
a shear band

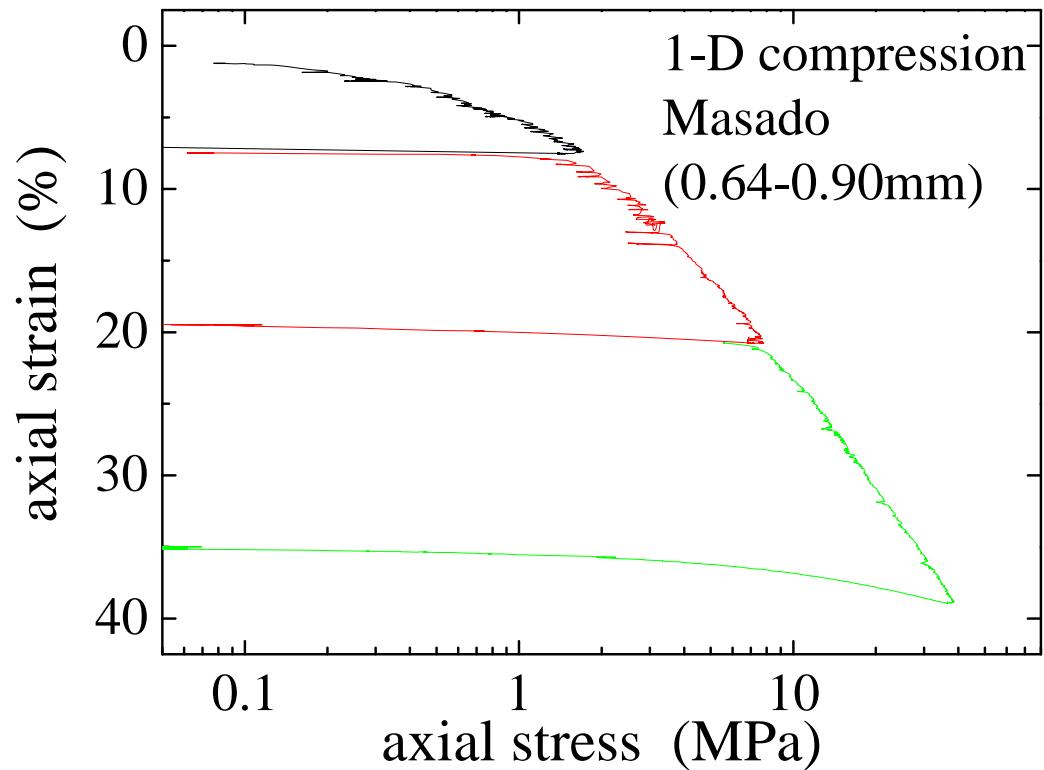
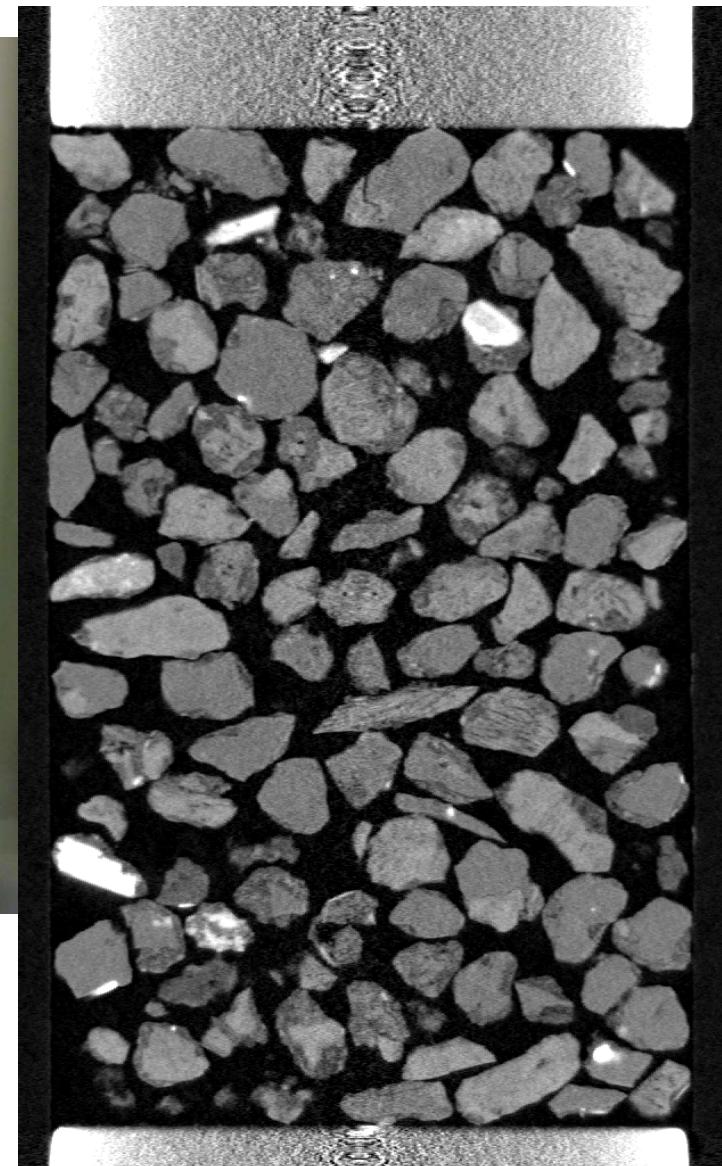
# Micro Triaxial test (BL20B2)(4)



Masado (cruchable sand)  
0.351-0.64mm  
(medium dense)

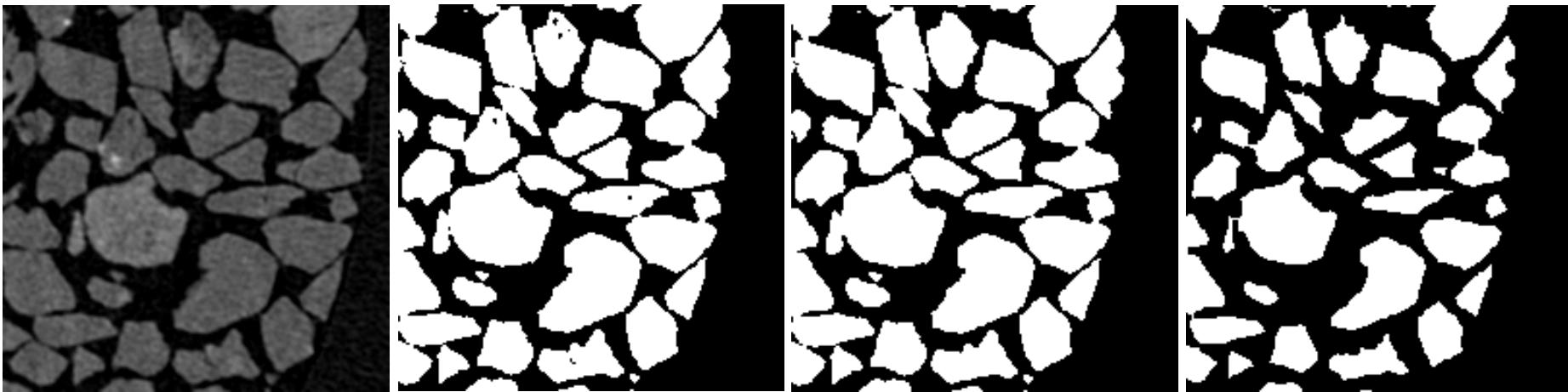
particle crushing is  
NOT predominant

# Micro 1-D compression test

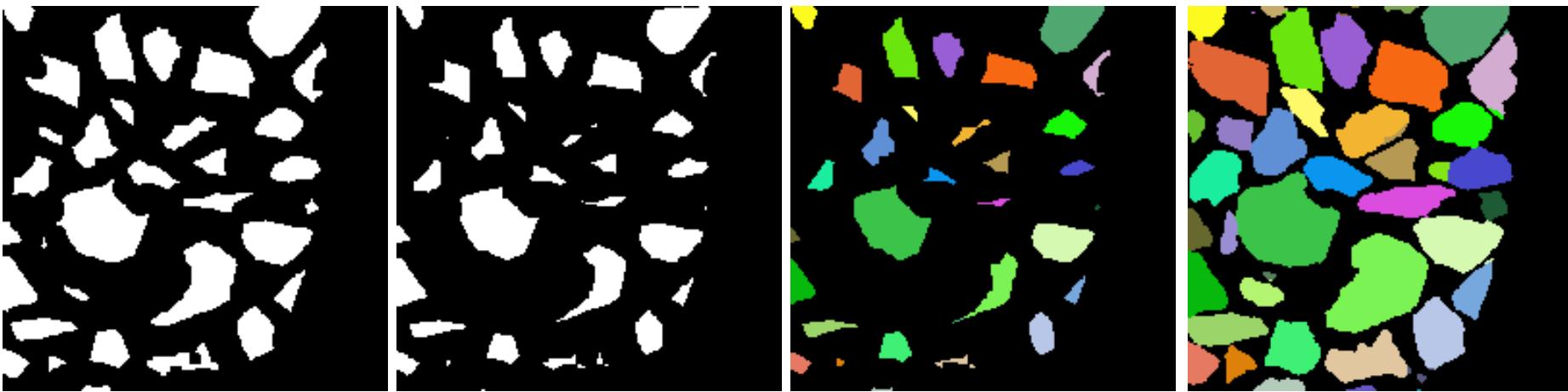


particle crushing  
after yield stress

# Processing of CT image

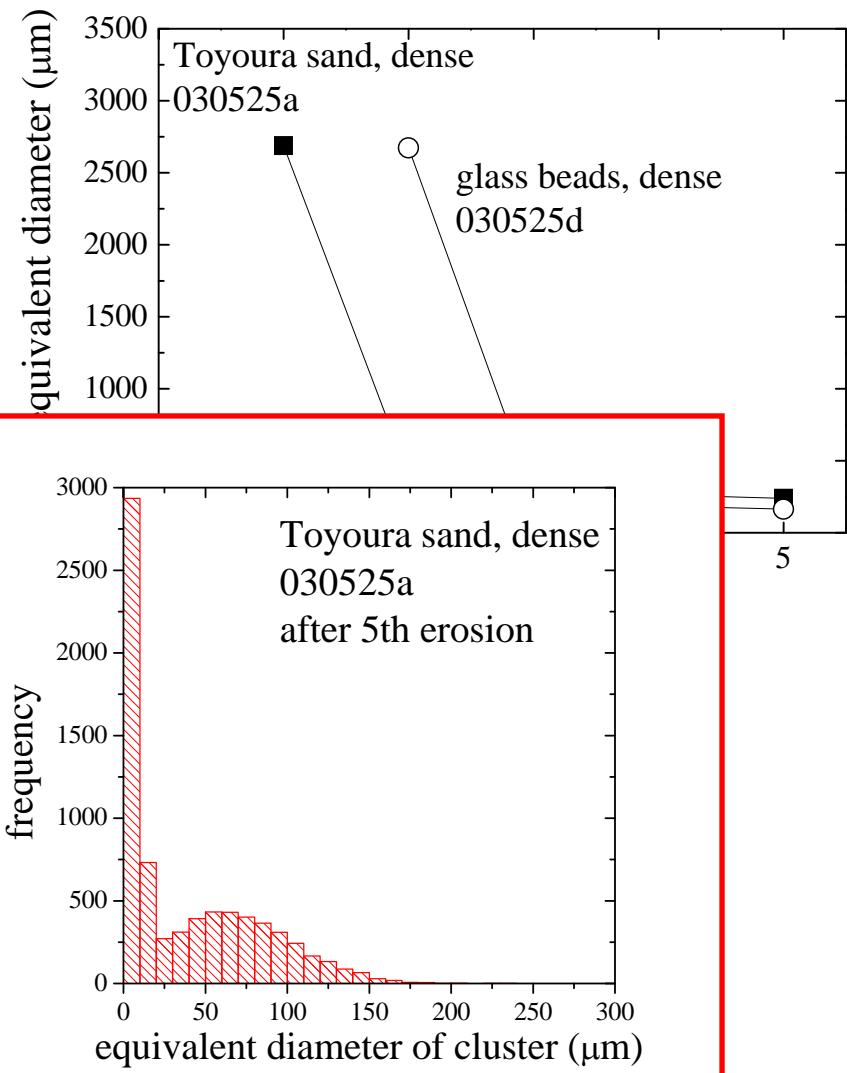
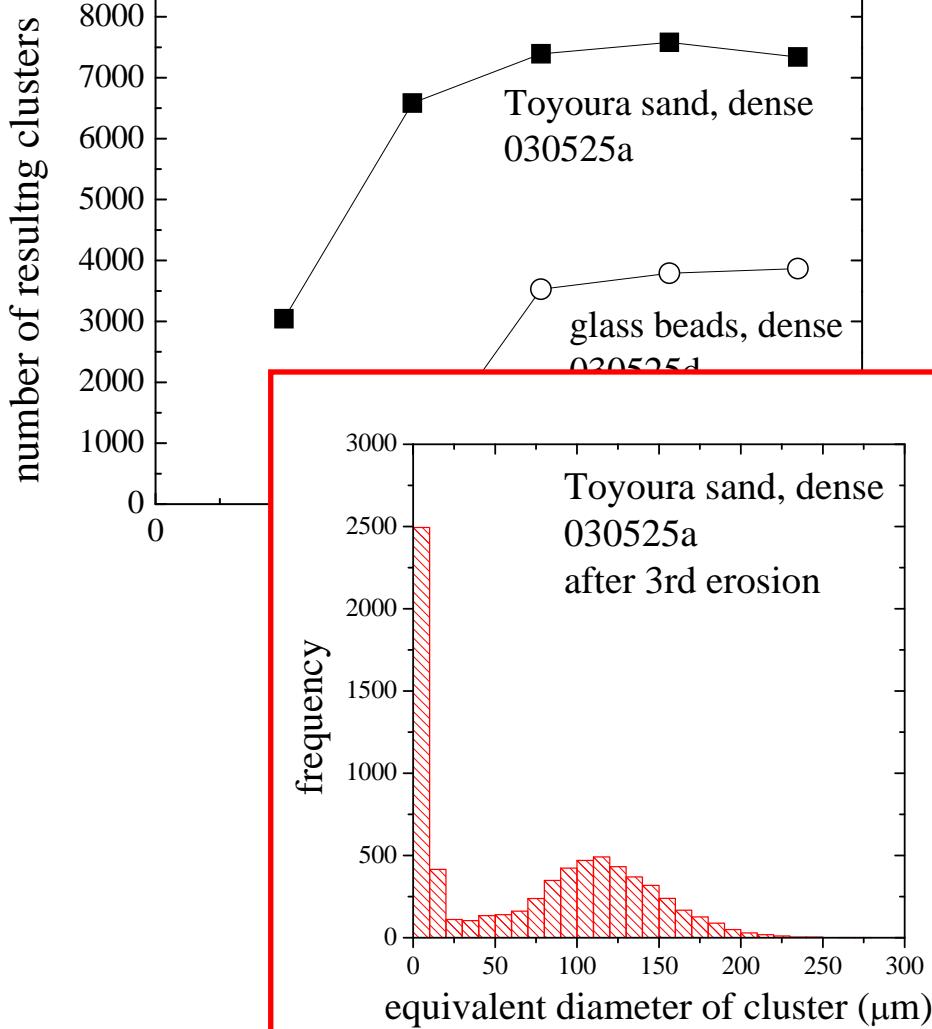


Original image   After binarization   After pore-filling   After 1st erosion

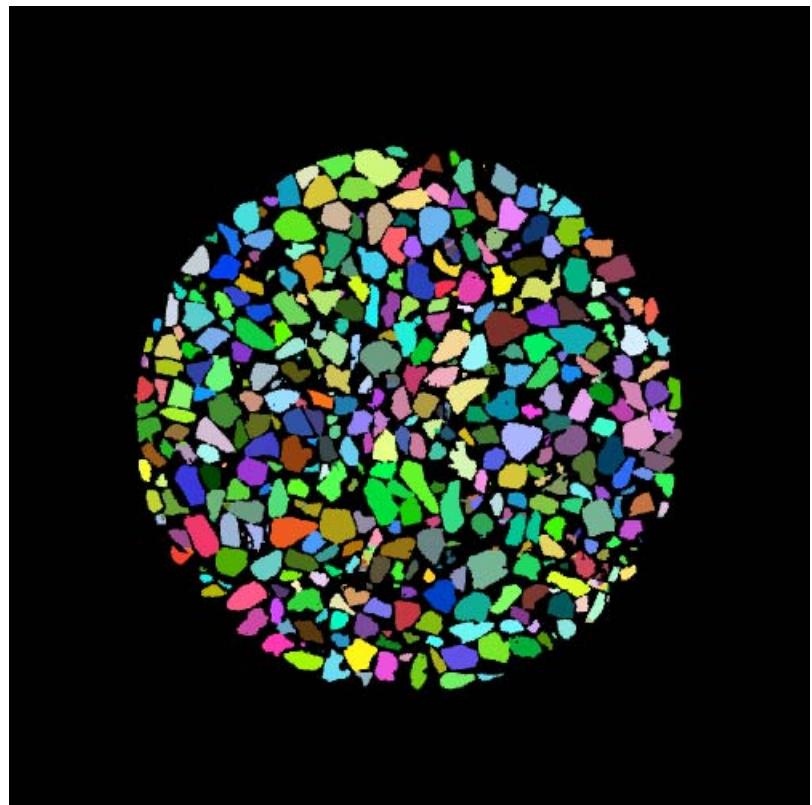
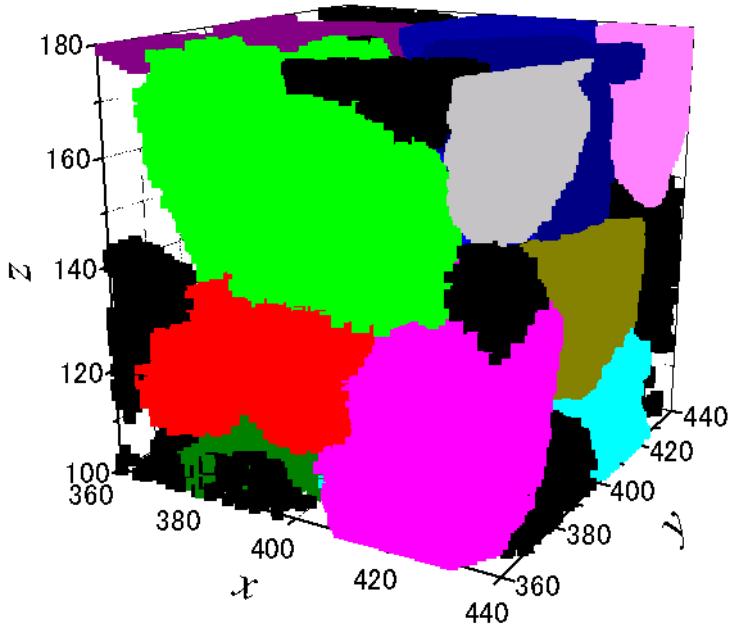


After 2nd erosion   After 3rd erosion   Cluster labeling   Attribution

# Adequate erosion cycles

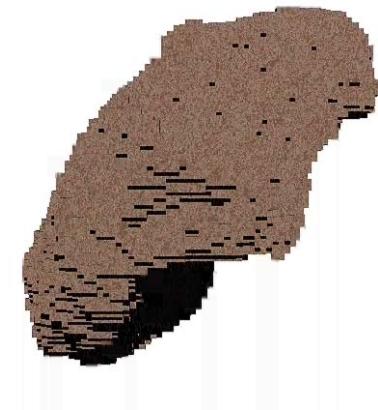
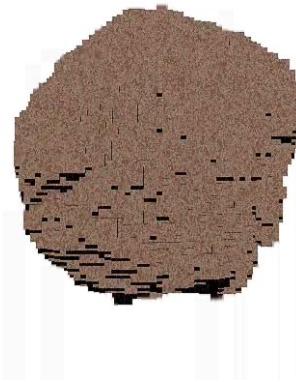
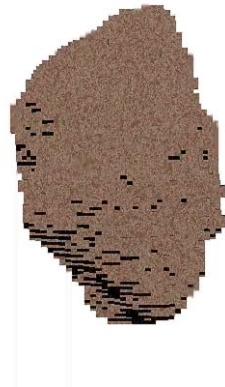
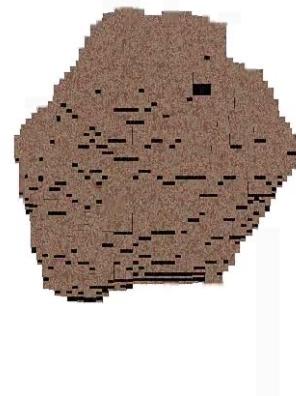
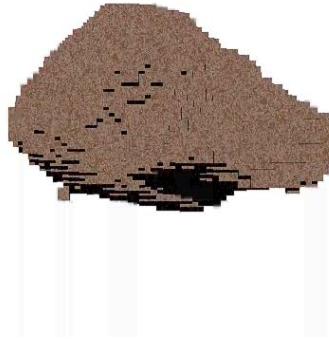


# Grain identification



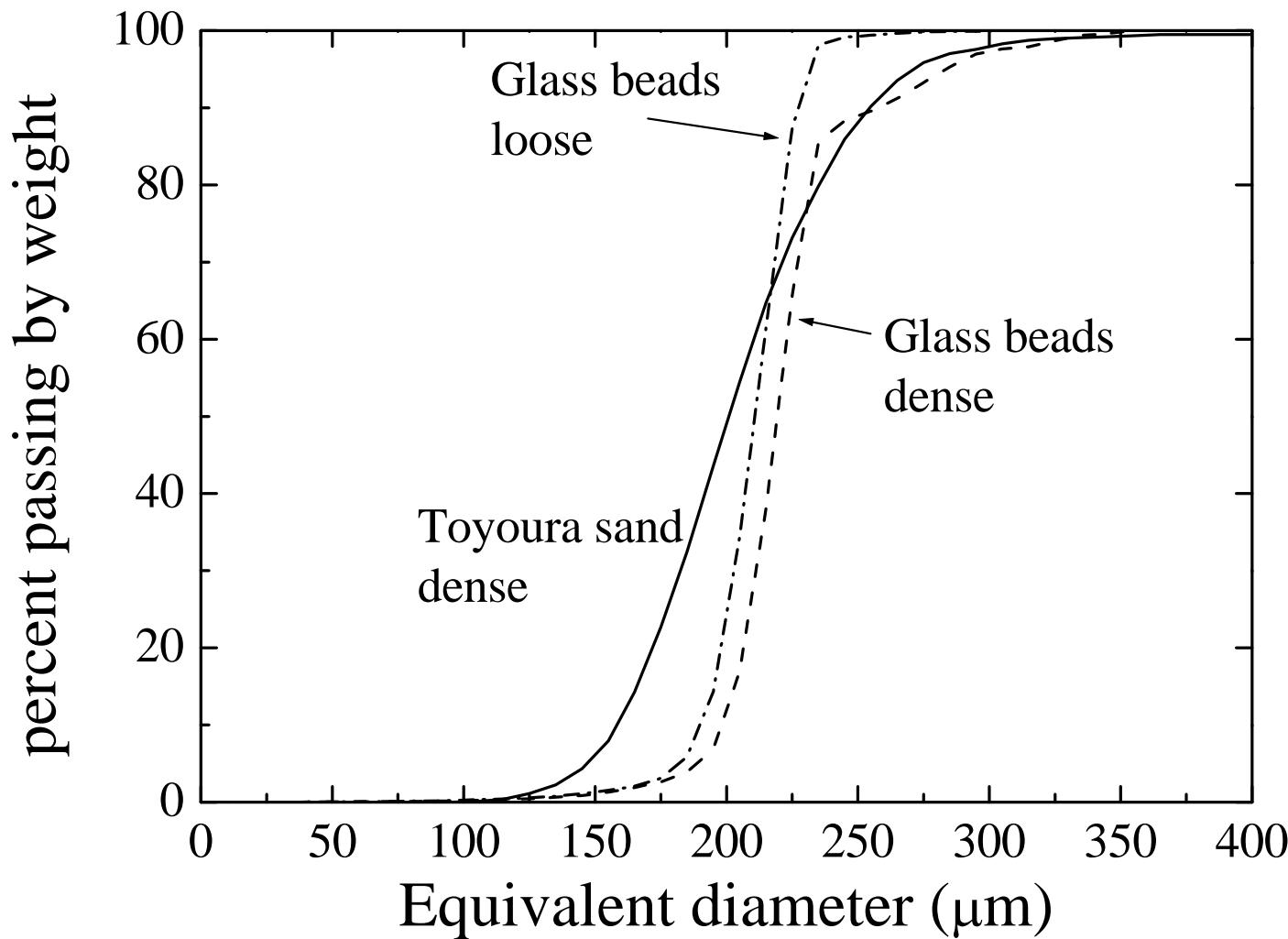
3-D image after attribution process

# Grain identification

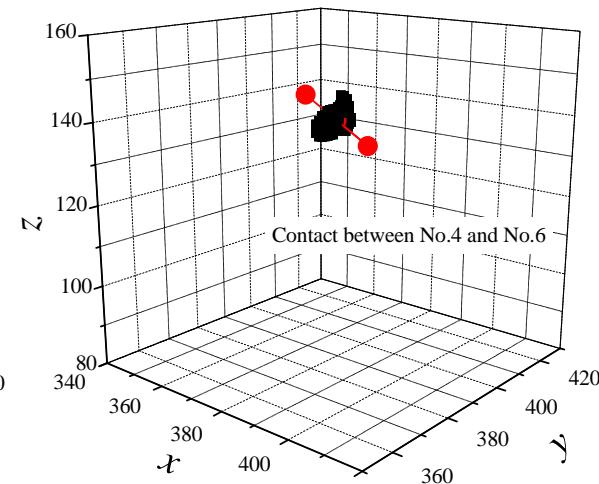
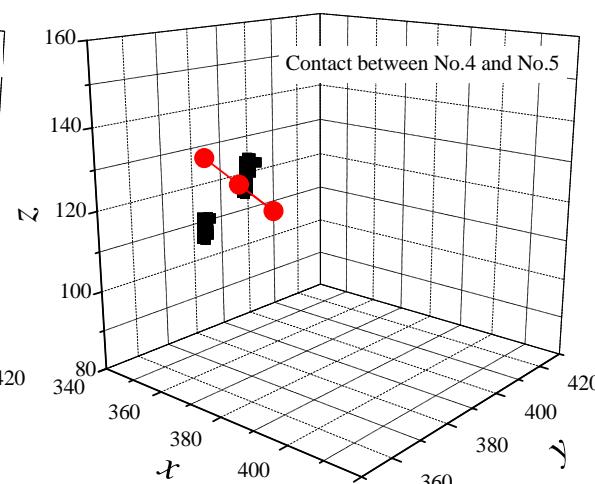
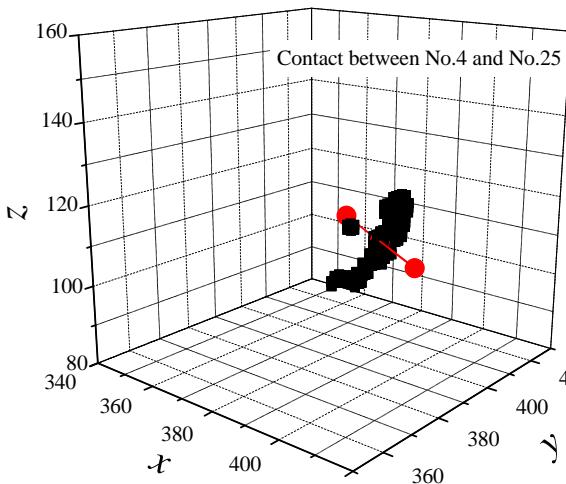
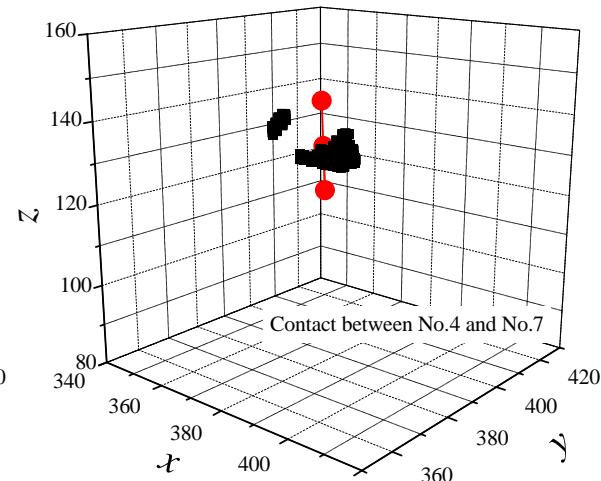
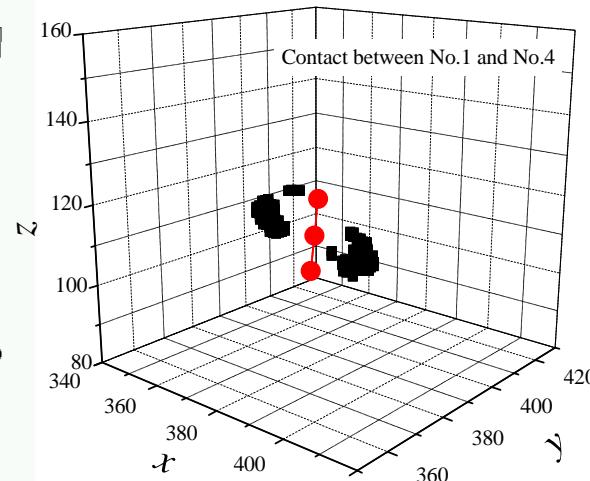
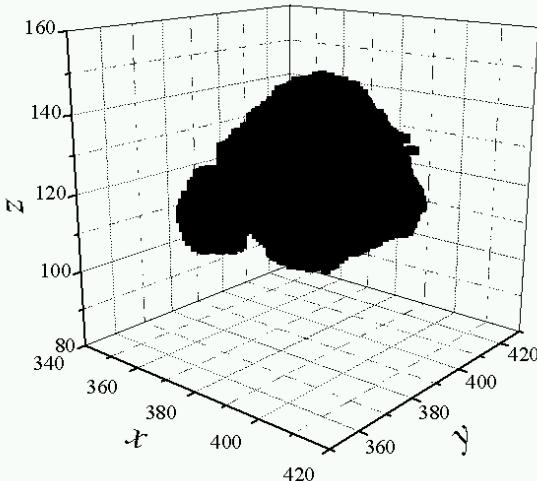


**Identified Toyoura sand grains**

# Grain size distribution

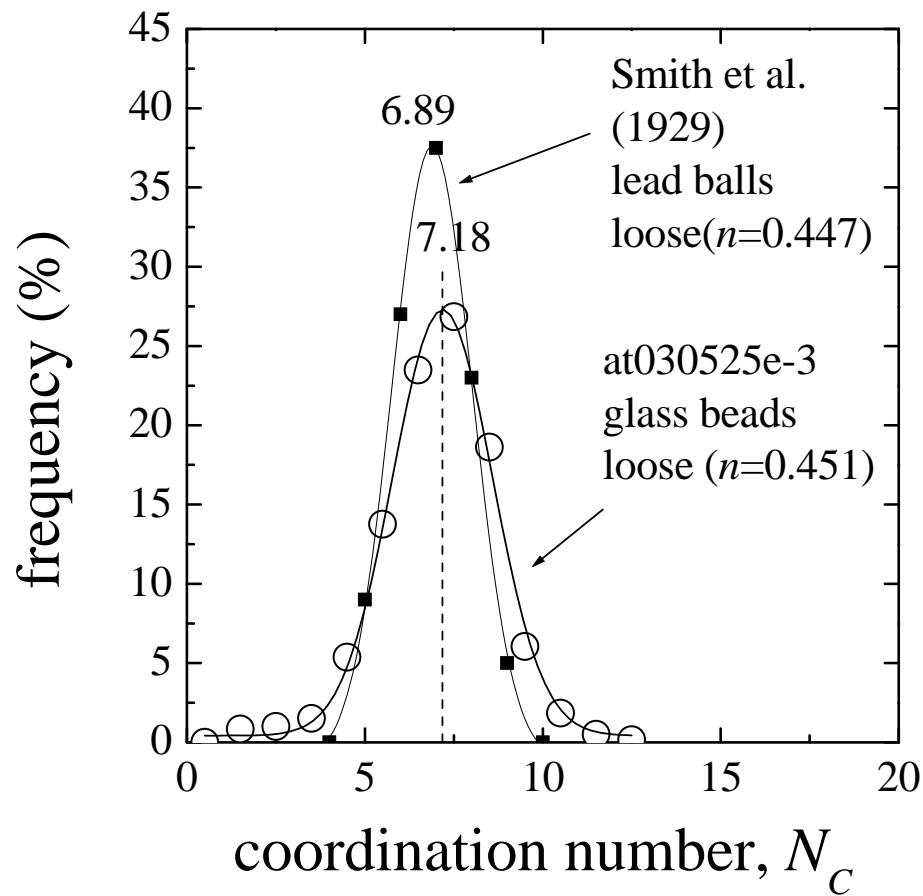
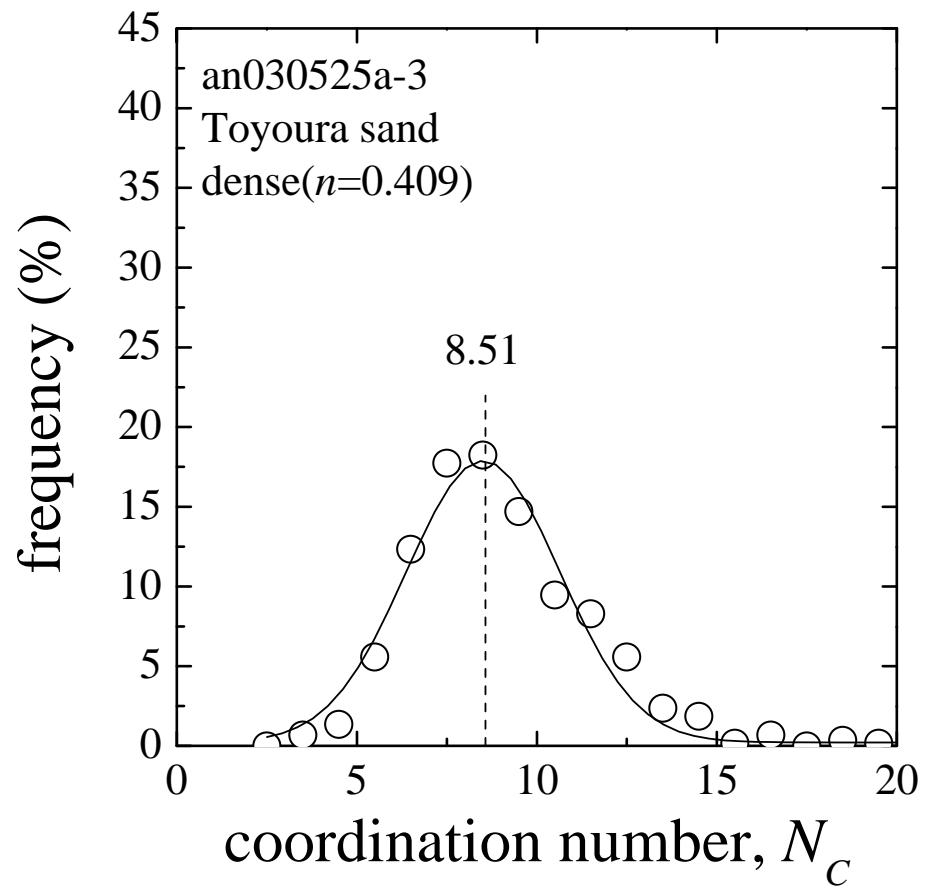


# Contact area and their normals



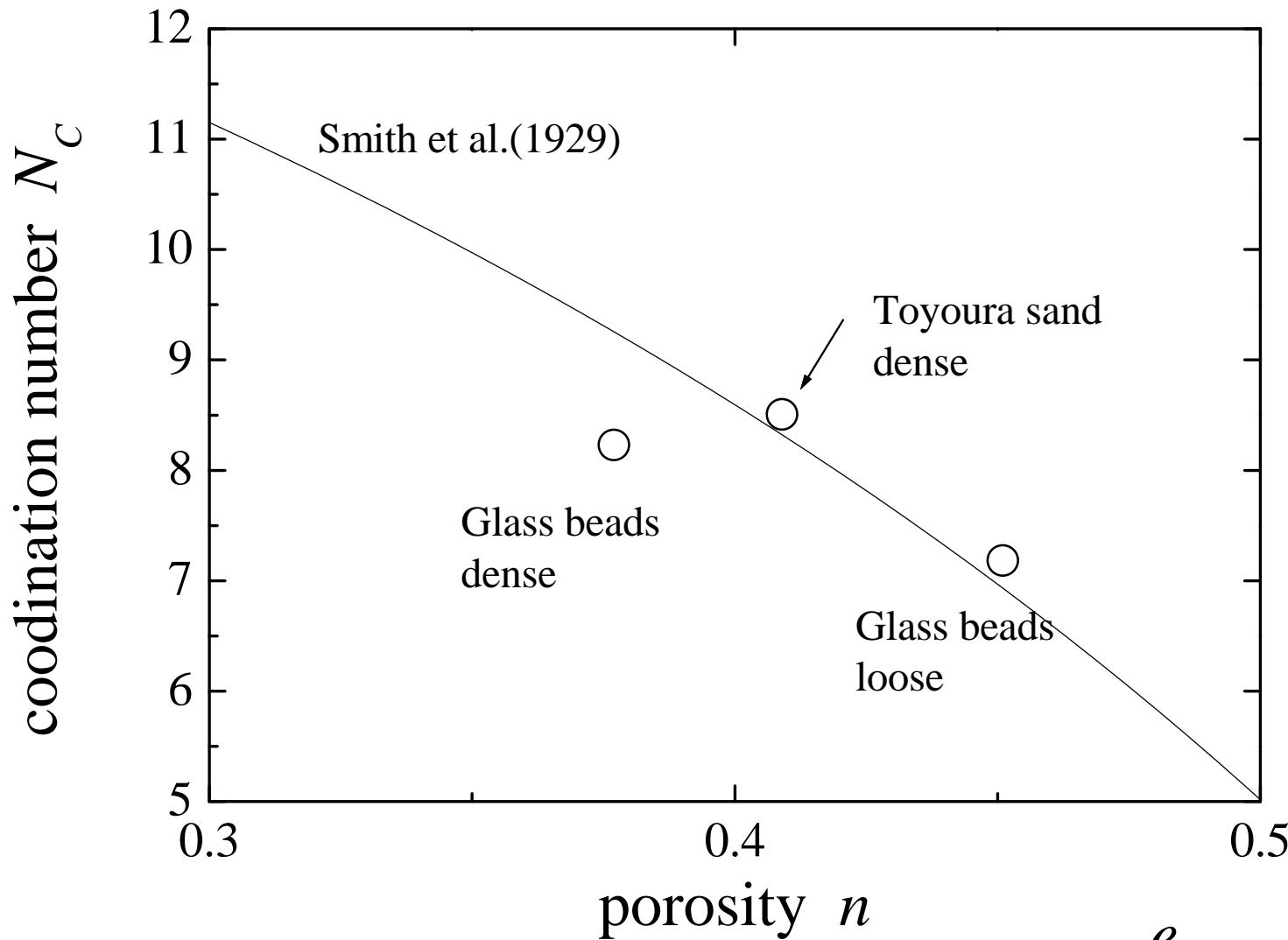
→ coordination number, fabric tensor, etc.

# Coordination number (1)



like a normal distribution

# Coordination number (2)



$$n = \frac{e}{e + 1}$$

# Next step

---

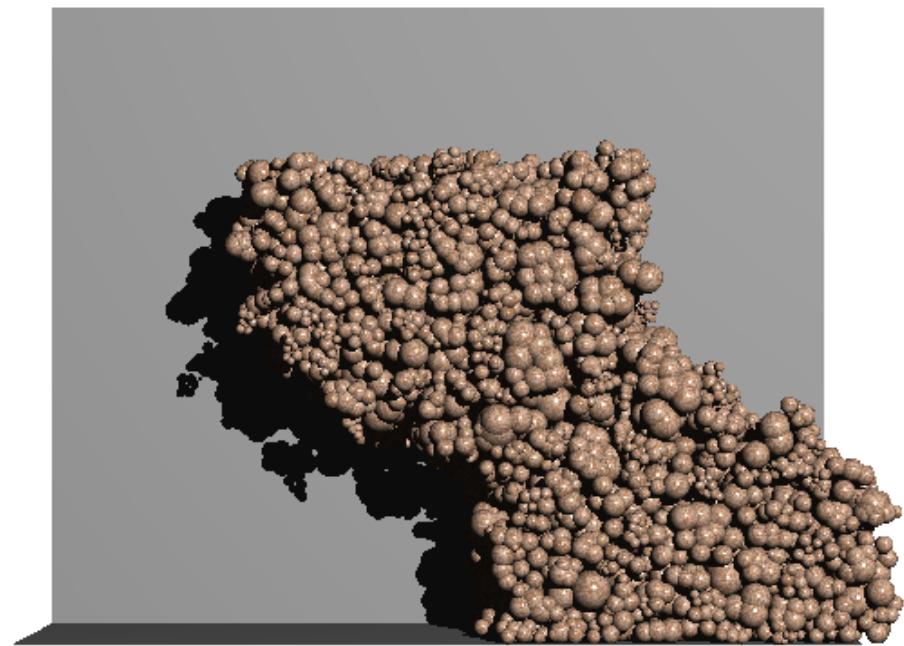
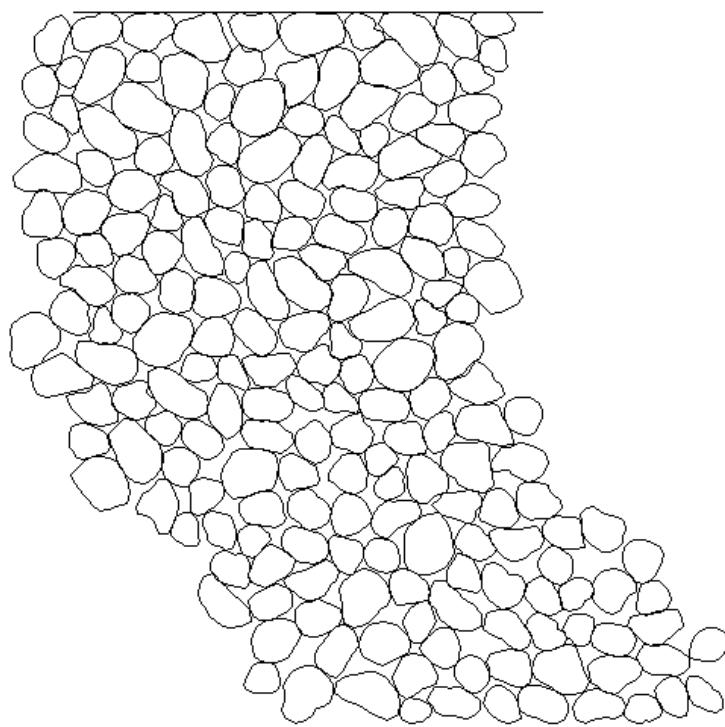
**\*Detection of each grain motion  
(translation and rotation)**

(Chang, Matsushima, Lee, J. Eng. Mech. ASCE, 2002.)

**\*Detection of grain crushing**

# Image-based DEM

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# Background

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- \* Rapid increase of computer abilities  
→ **DEM** simulations with large number of grains
- \* For **quantitative** discussion...  
→ **Precise modeling** of grains  
(contact model, grain shape, crushability, etc.)  
is necessary.

This study deals with

**GRAIN SHAPE MODELING**

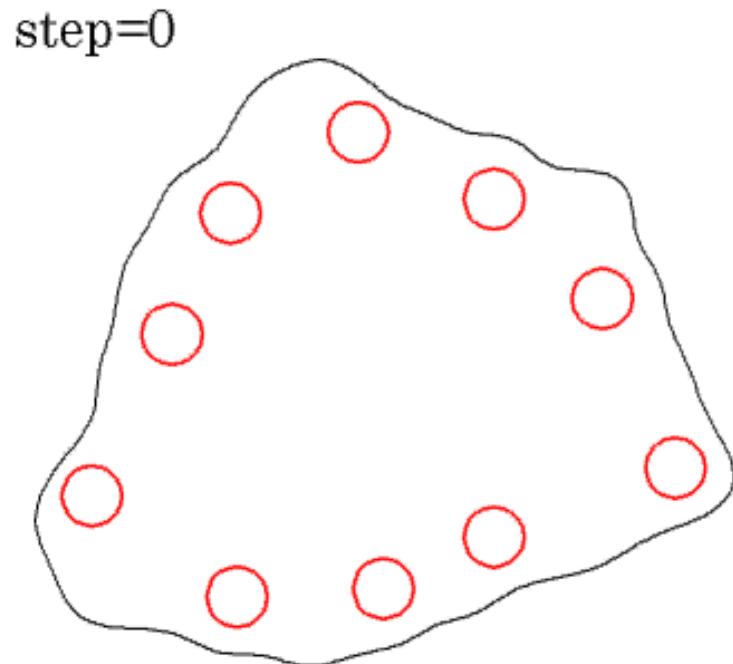
# Image-based modeling (Matsushima and Saomoto 2002)

Irregular grain shape is described by a **rigid connection of elements** (circles or spheres)

To find an **optimum positions and radii** of the elements...

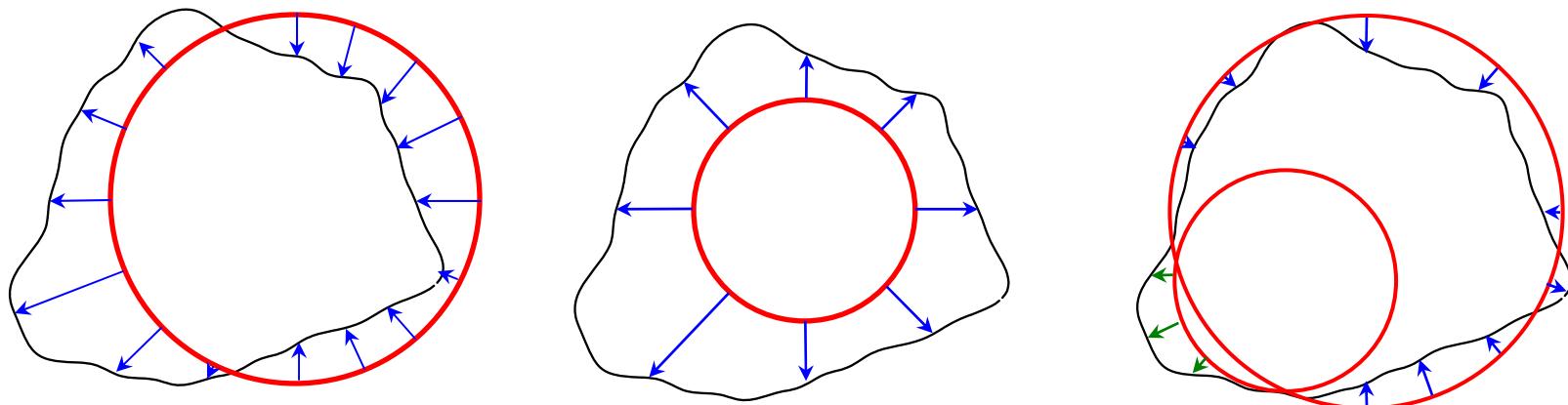
time marching computation  
(Dynamic optimization)

Each element moves and expands (or shrink)  
to get a better fitting to the target grain shape

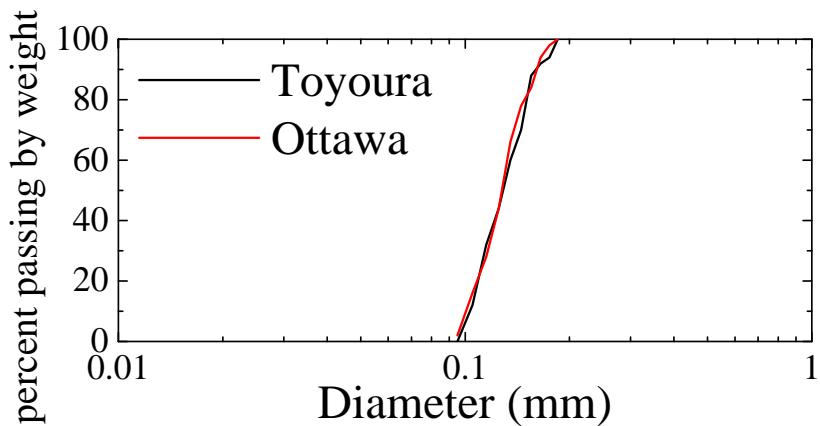


# Dynamic Optimization algorithm

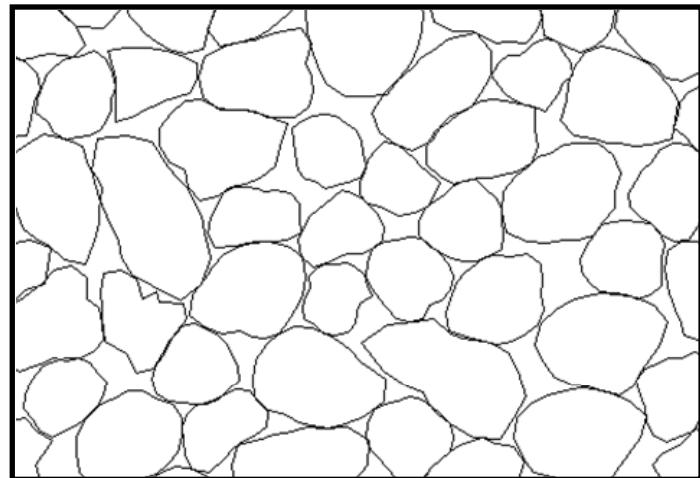
Each surface point of a target grain gives an **attraction** to the closest element which directs from the centroid of the element to the surface point and its magnitude is proportional to the distance.



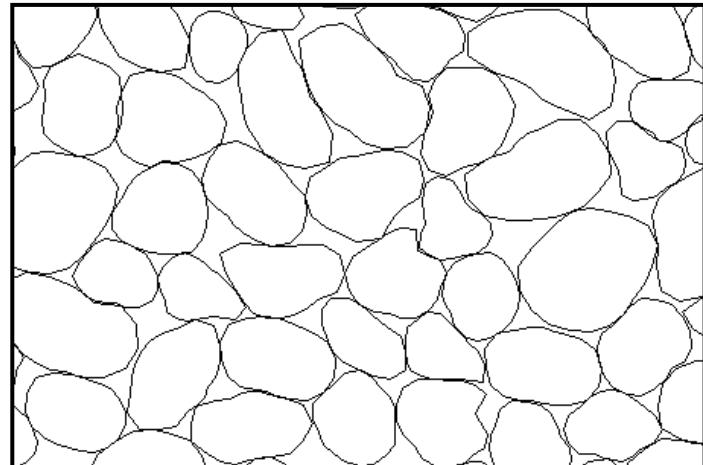
# 2D example (1)



Grain density	2.64(g/cm <sup>2</sup> )
Spring constant (normal)	1.0e9 (g/s <sup>2</sup> )
(tangential)	2.5e8 (g/s <sup>2</sup> )
Damping coefficient (normal)	2.0e2 (g/s)
(tangential)	1.0e2 (g/s)
Friction coefficient between grains	27 (deg.)
Time increment	2.5e-8 (sec.)

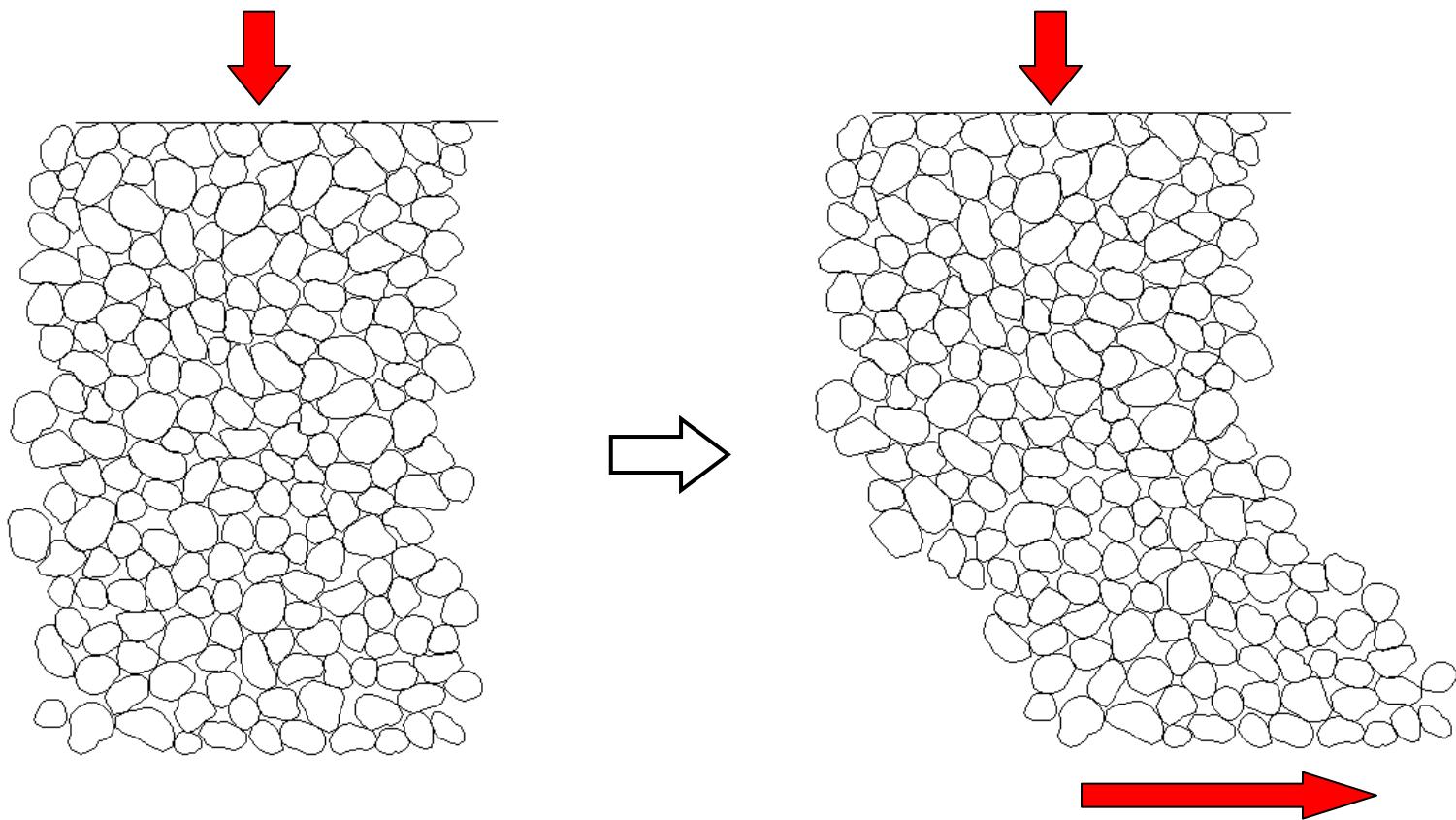


Toyoura sand (sub-angular)



Ottawa sand (sub-rounded)

## 2D example (2)



**200 grains (Each grain is modeled with 10 elements)**

**Periodic boundary** at both sides

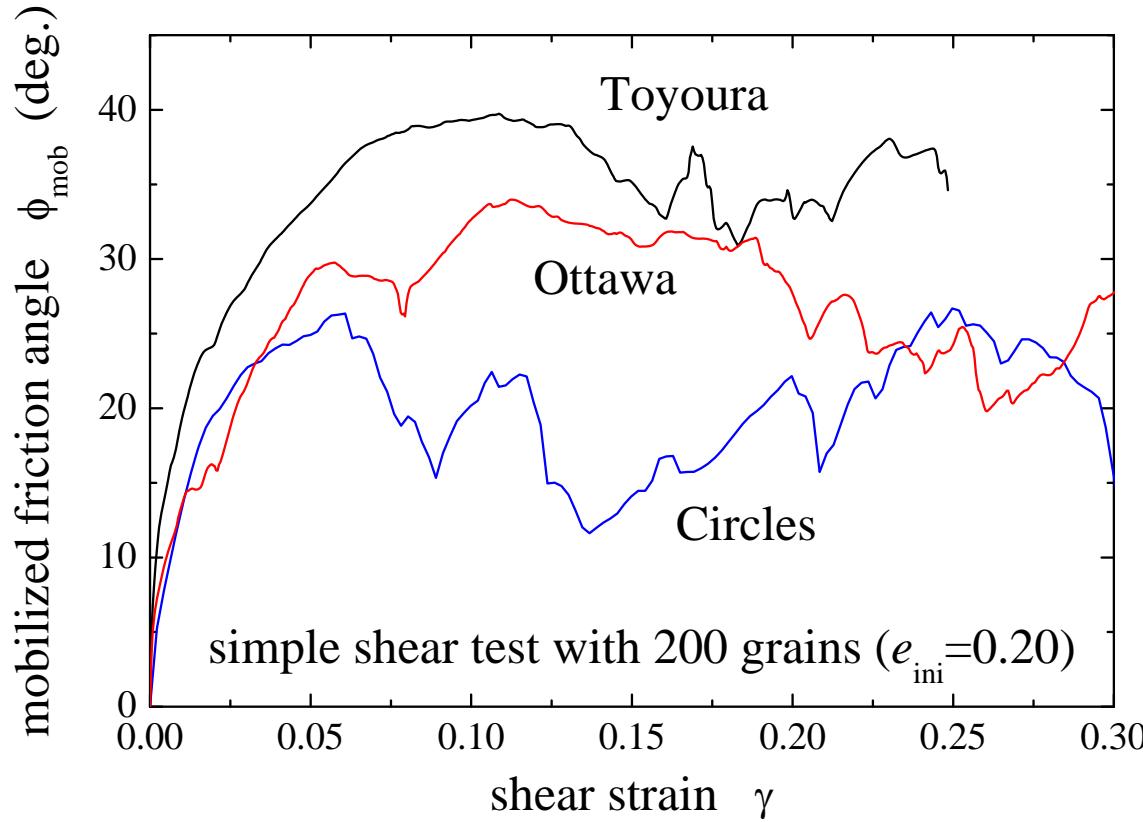
**Constant confining pressure(10kN/m),**

**Lateral displacement is imposed at the bottom grains**

# 2D example (3)

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Dense specimen ( $e_{ini}=0.20$ )

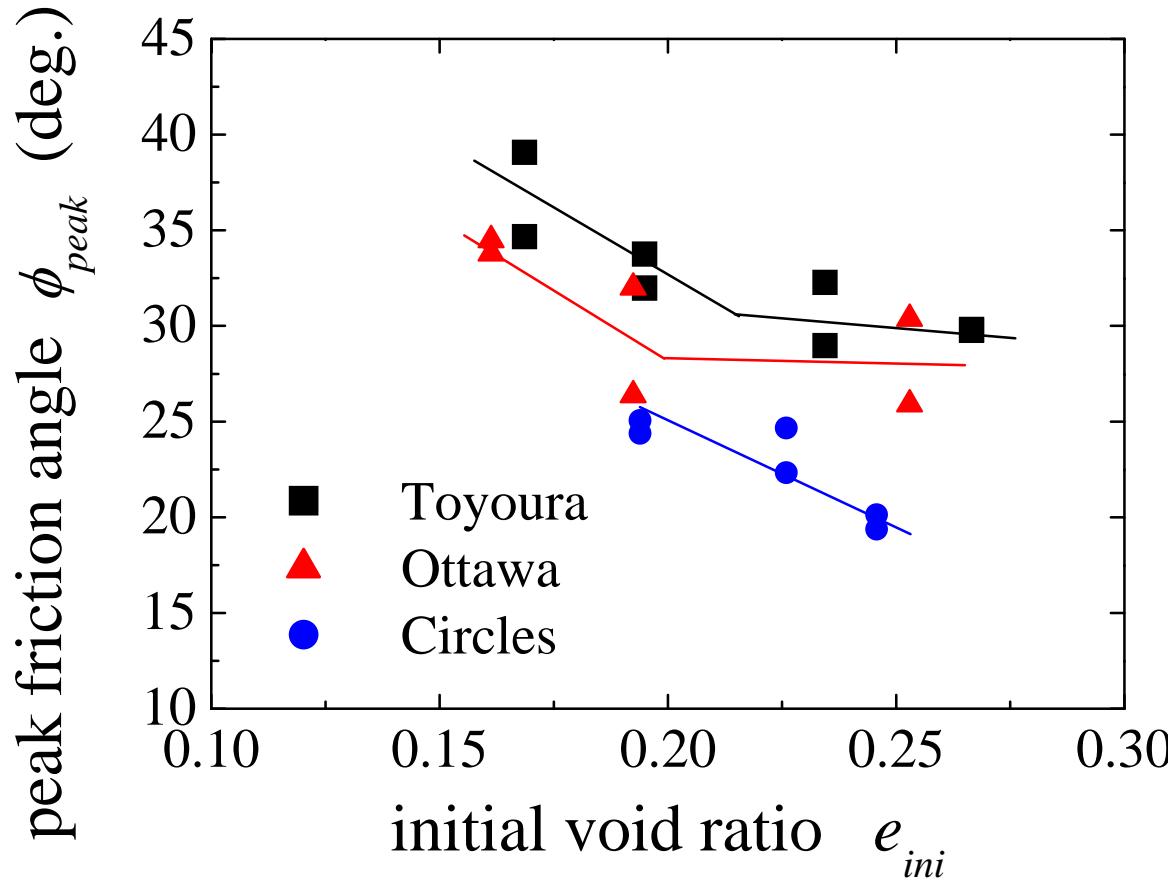


Toyoura>Ottawa>Circles for peak strength

## 2D example (4)

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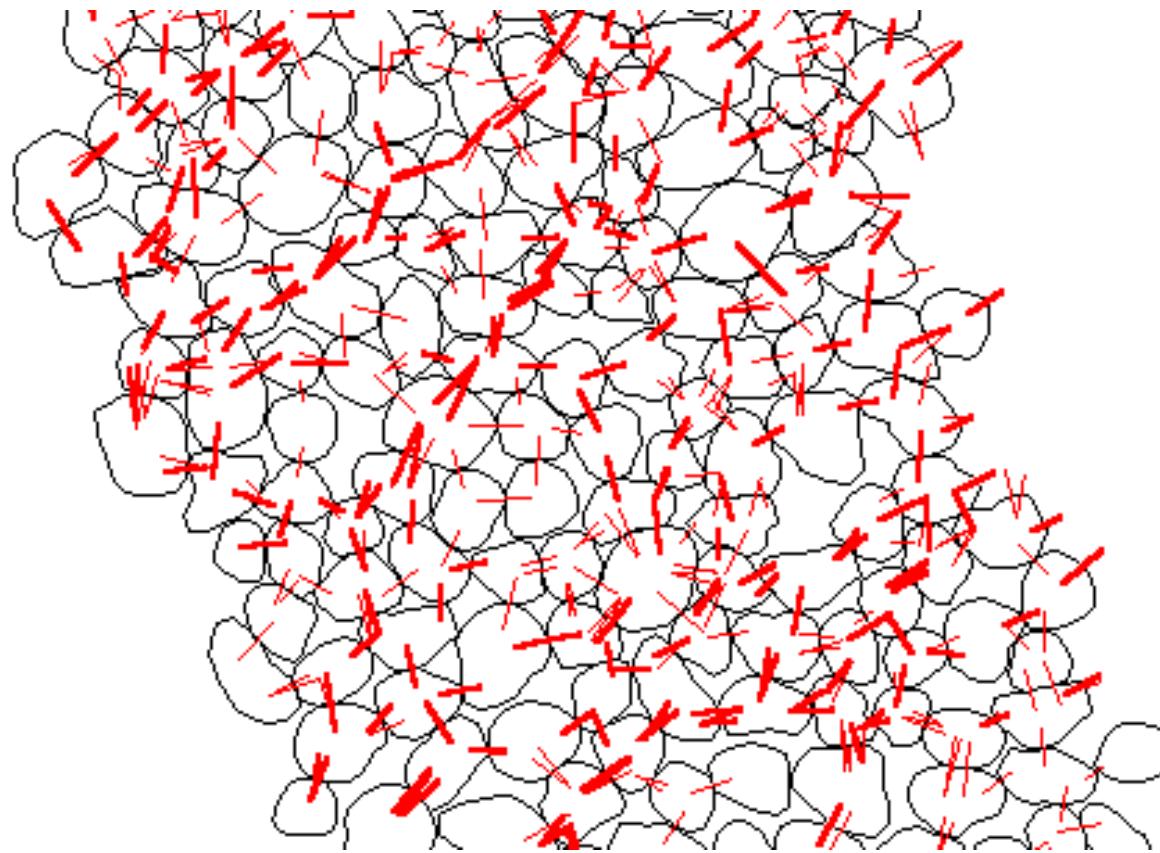
### Peak strengths with different initial void ratio



The modeling is verified qualitatively.

## 2D example (5)

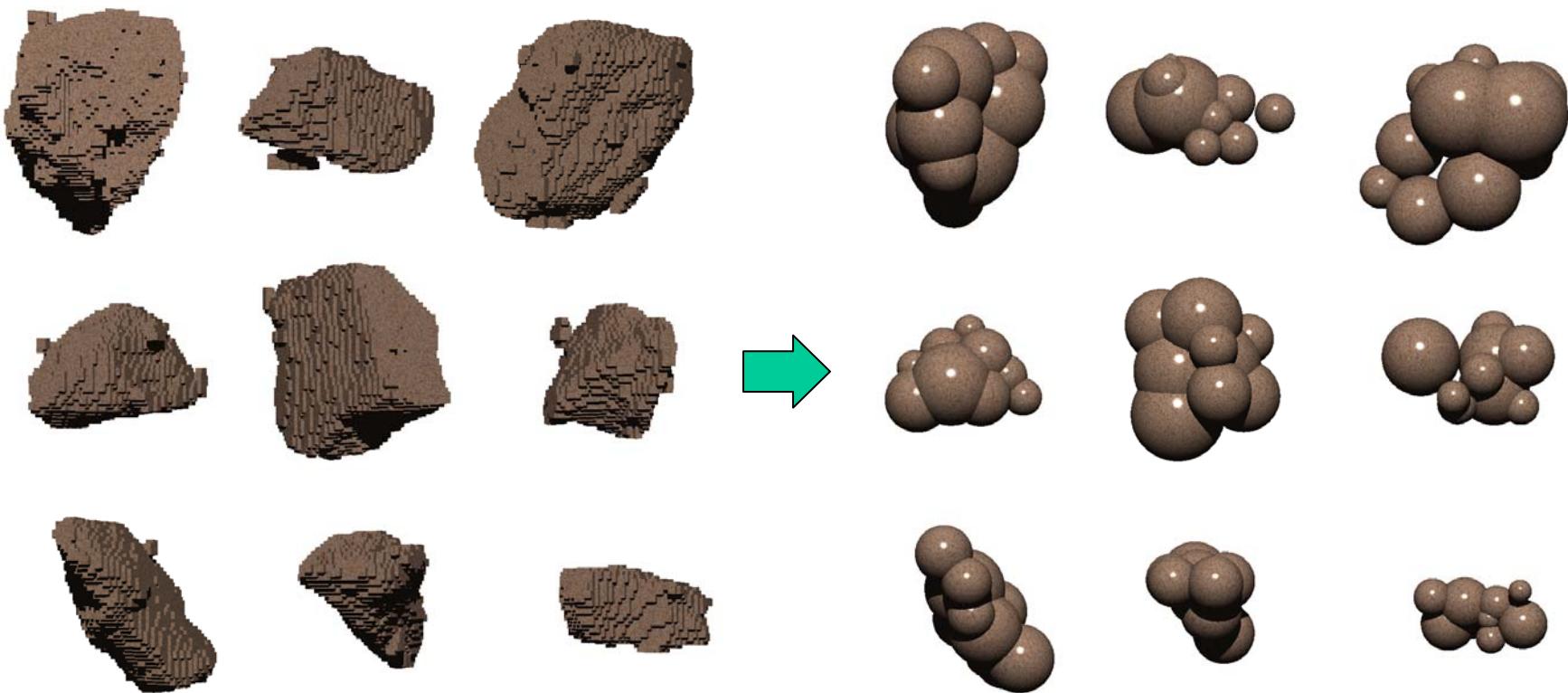
### Granular column structure during shear



Two grains are in contact with plural points  
→ Moment transmission → Higher strength

# 3D example: Toyoura sand (1)

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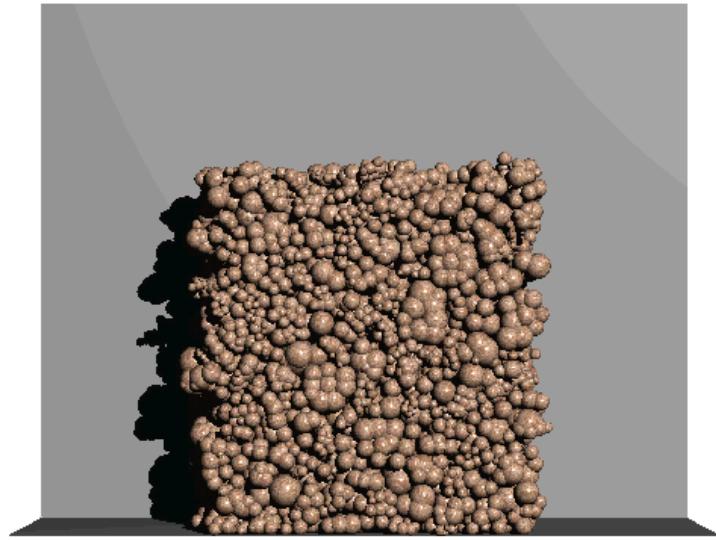
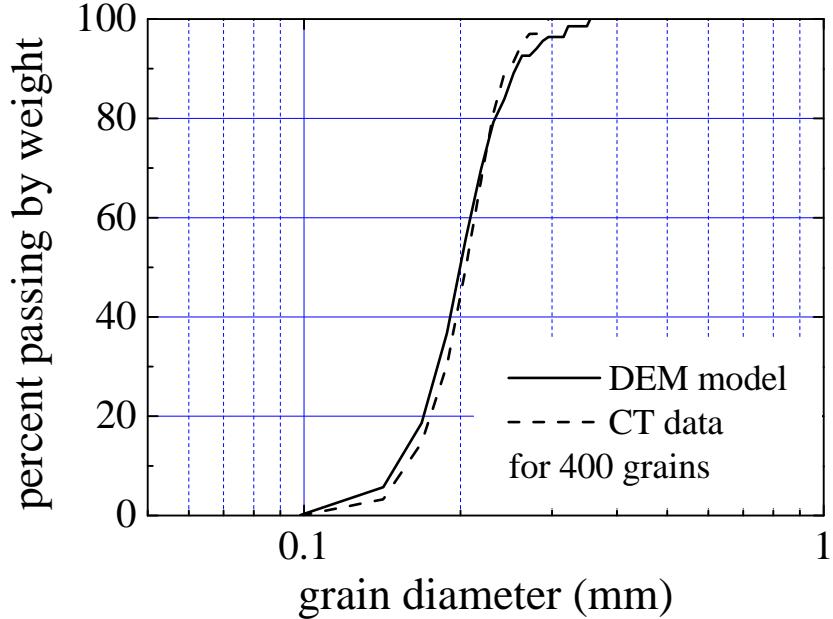


X-ray CT result

3D modeling

Toyoura sand model

# 3D example: Toyoura sand (2)

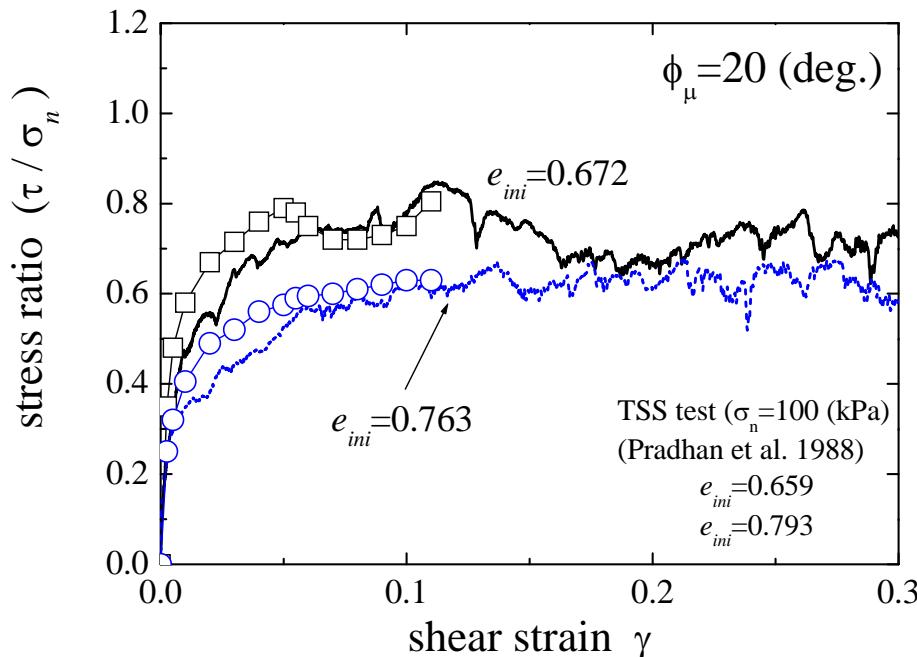


**Grain size distribution:**

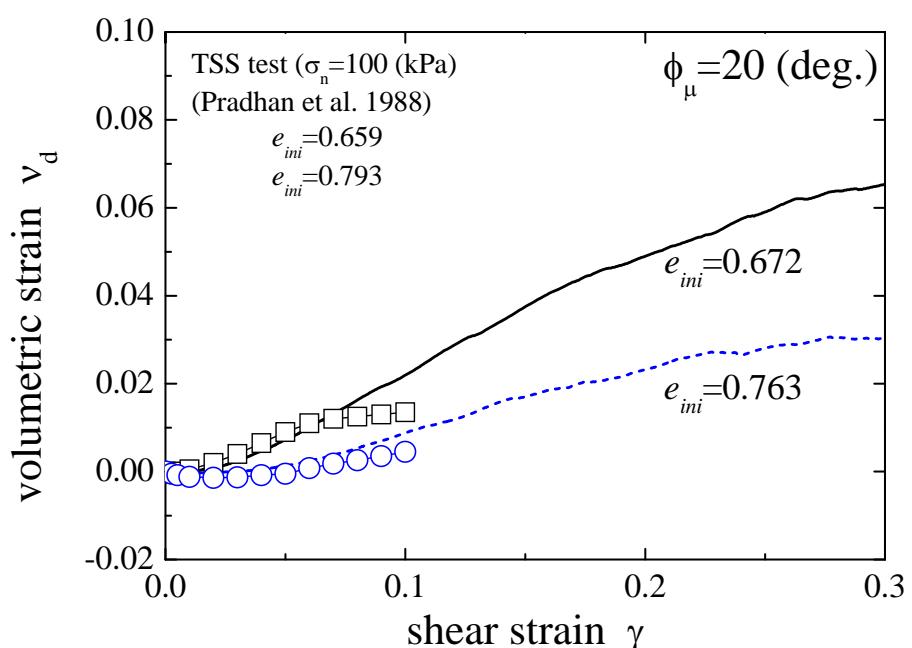
**DEM model = original CT data**

**Simple shear simulation**

# 3D example: Toyoura sand (3)



Stress-strain curve

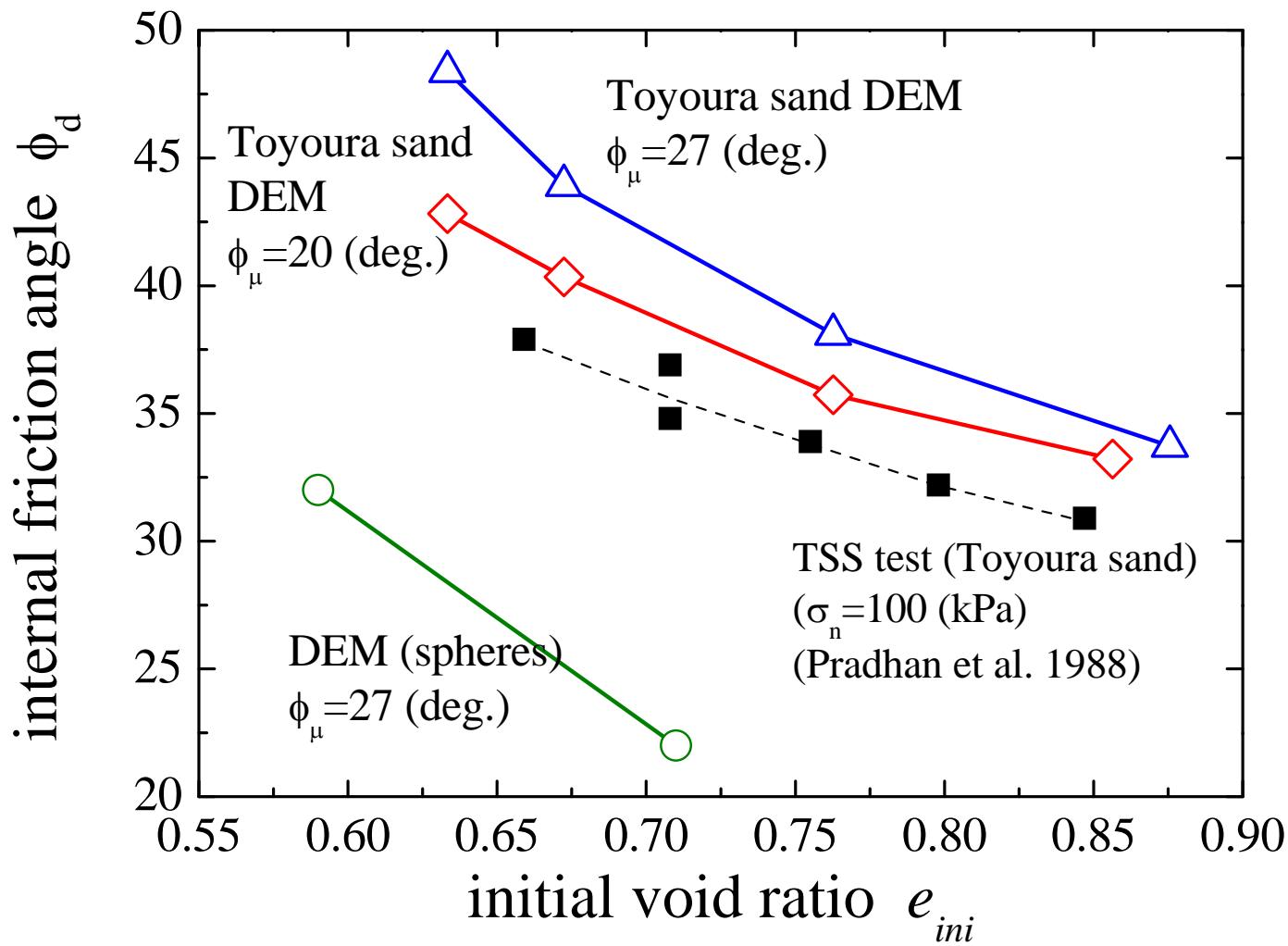


dilation curve

Quantitative agreement with experiment  
if inter-particle friction angle=20(deg.)

# 3D example: Toyoura sand (4)

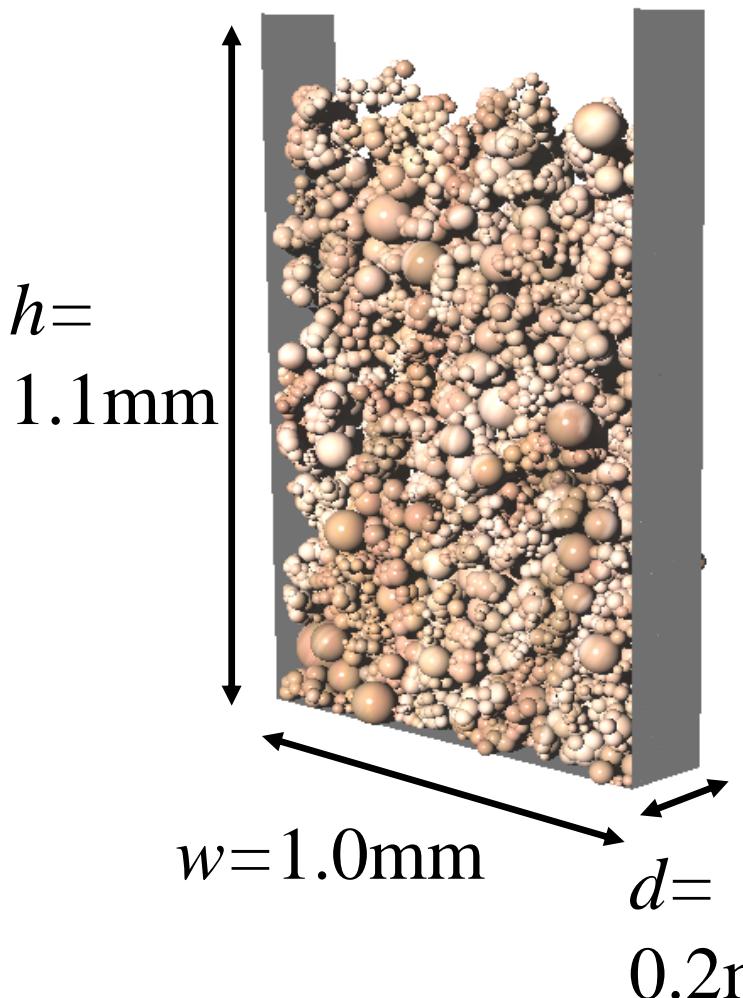
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**Peak strength for various void ratio**

# Lunar soil simulant (1)

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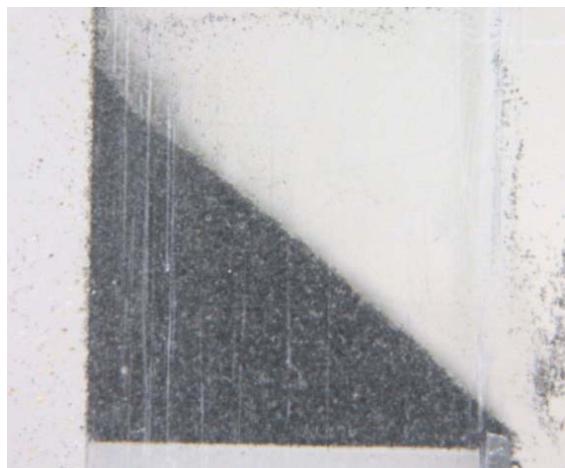
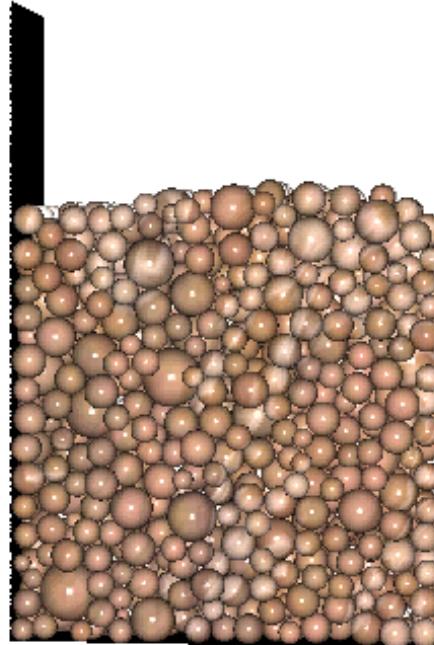
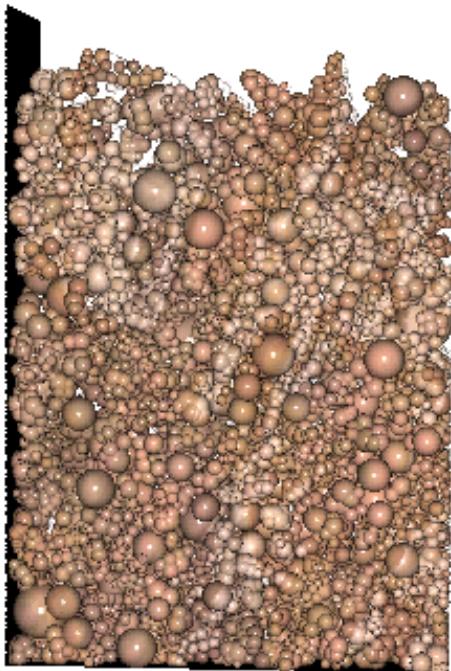


600 grains (10-spheres model)  
are fell down into a vessel

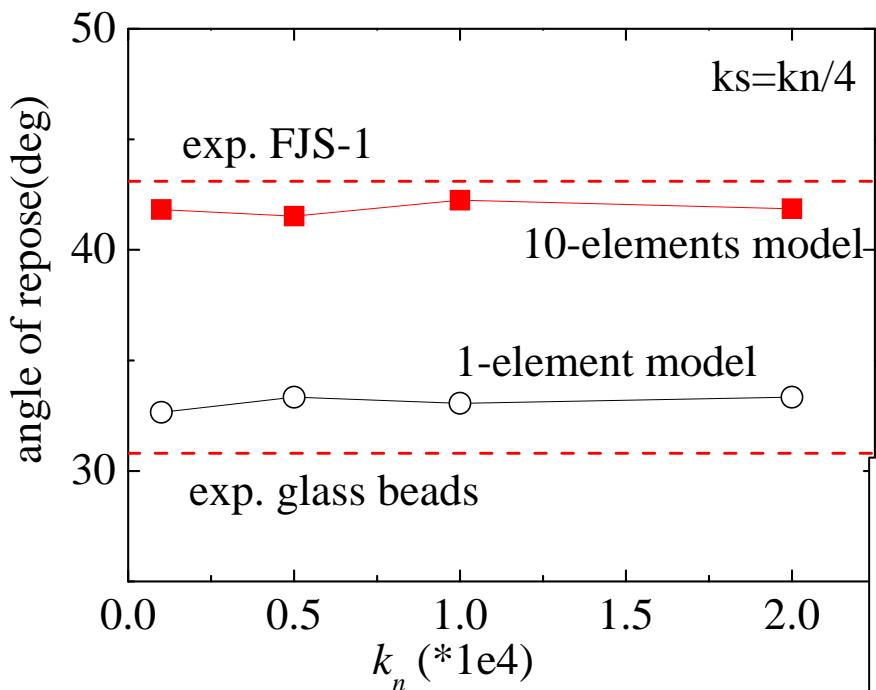
Periodic boundary in y-direction

Bottom grains are fixed into  
the bottom plate

Remove the right side wall

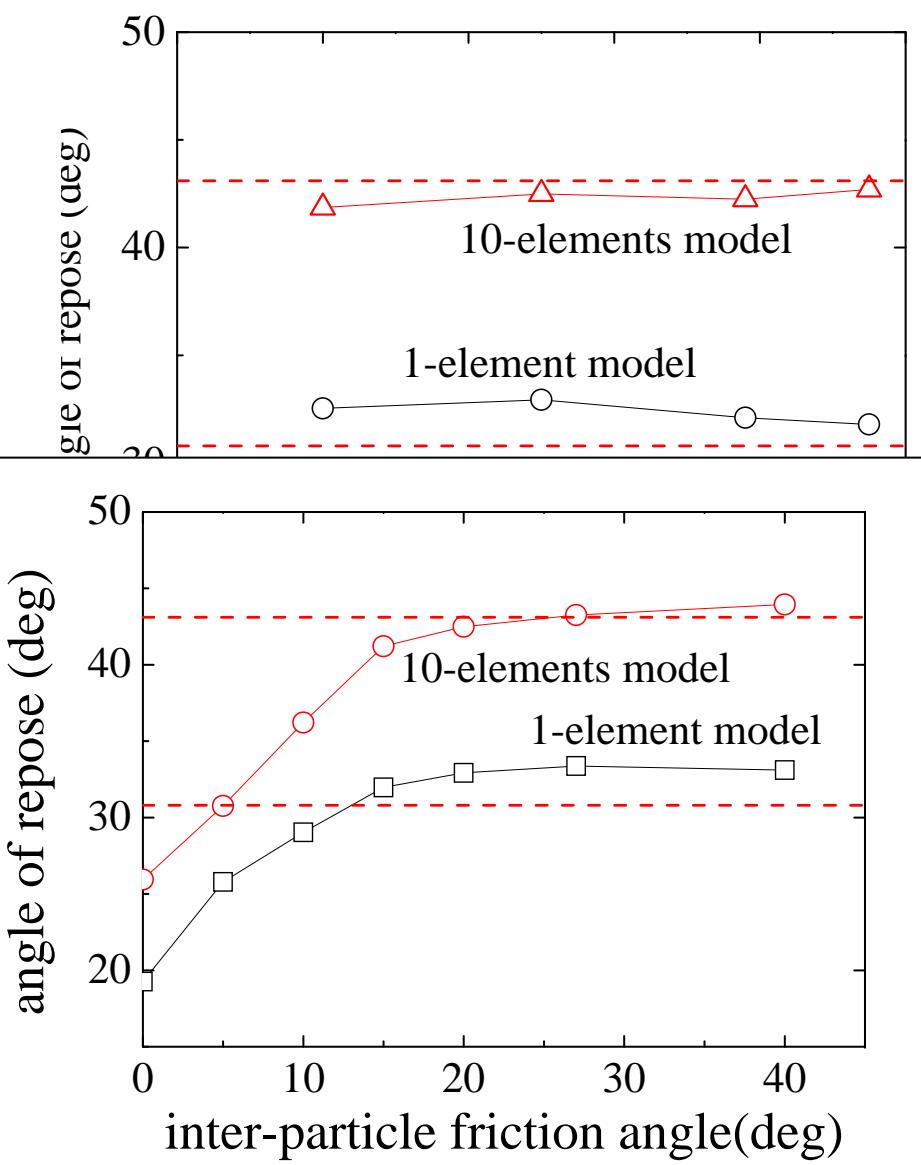


# Lunar soil simulant(3): Parametric study



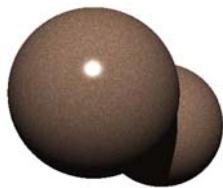
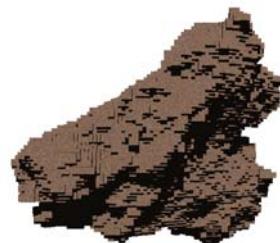
**Effect of grain hardness**

**effect of interparticle friction**

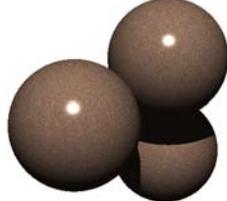


# Lunar soil simulant(4): model accuracy

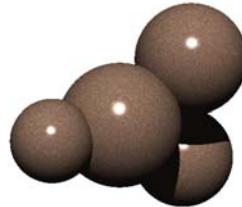
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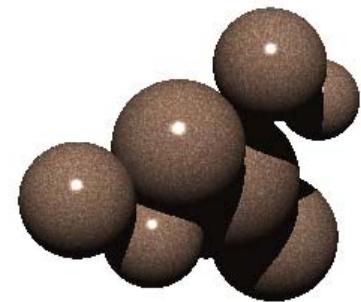
2-elements  
model



3-elements  
model



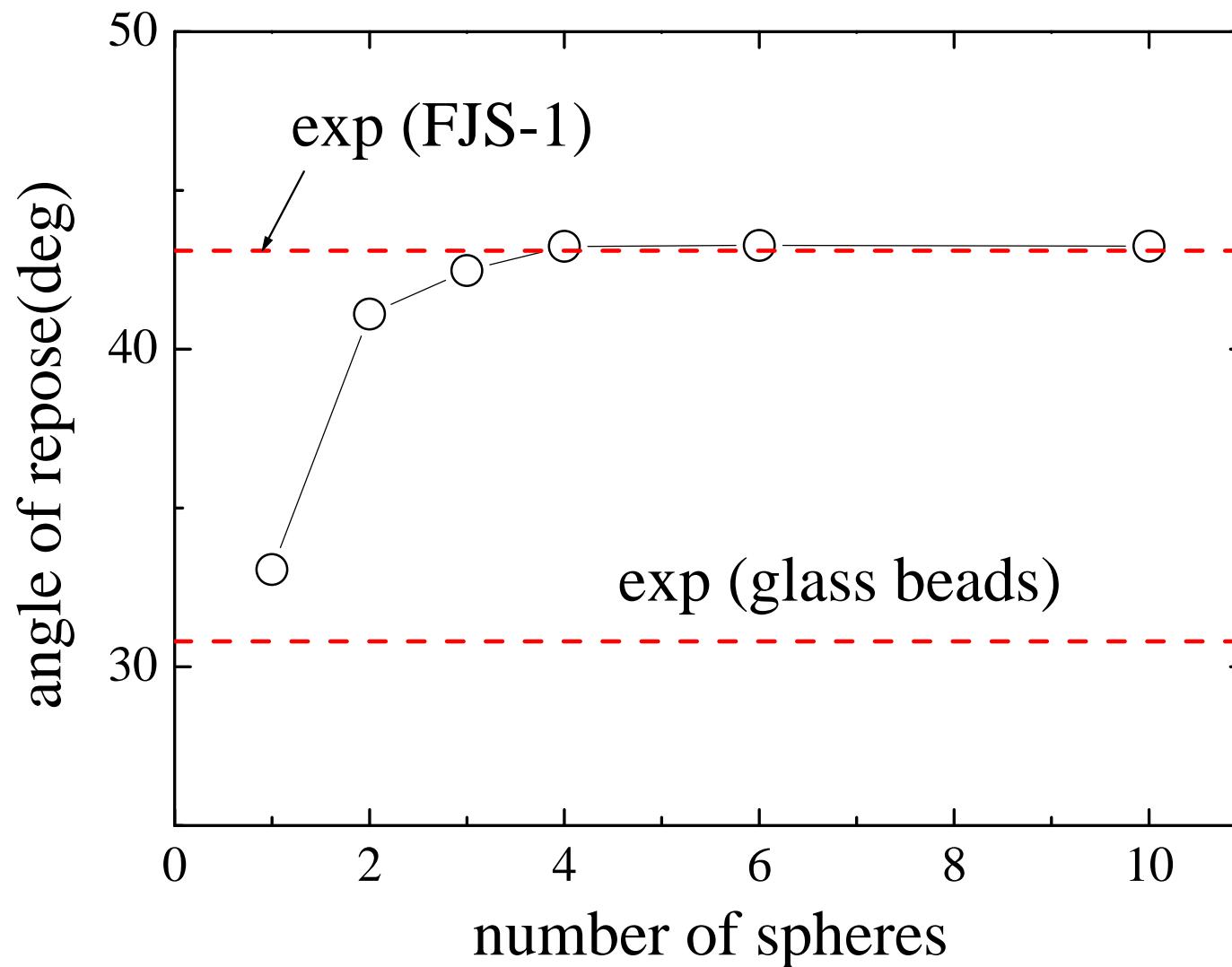
4-elements  
model



7-elements  
model

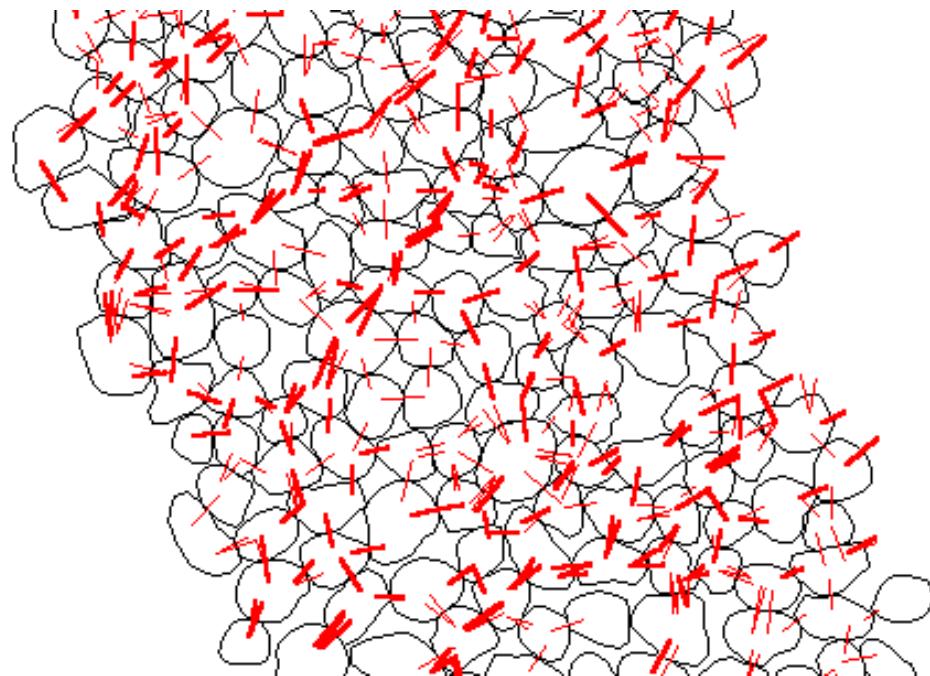
# Lunar soil simulant(5): model accuracy

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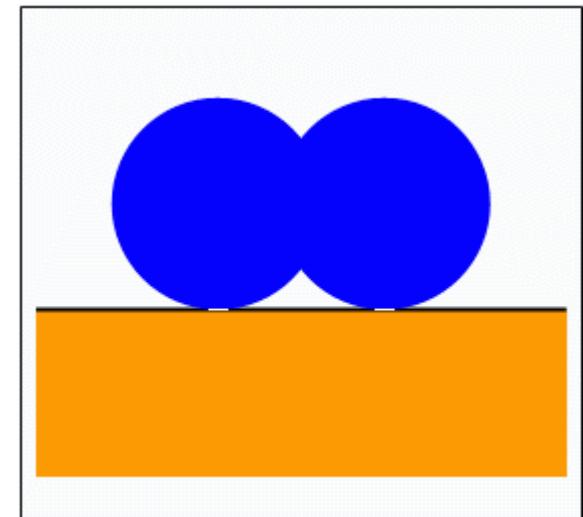


# Particle shape effect: The mechanism

## Contact force chain



Matsushima, P&G2005



**Plural contact points between two grains**  
→ **rolling resistance**  
→ **overall shape is important**



# Conclusions

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**Application of Granular Mechanics into geomaterials has been tried for decades.**

**Some breakthrough has been found recently (in my opinion).**

**Recent progress of various technologies makes it push forward.**

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